

## Thermomechanical properties of a single hexagonal boron nitride sheet

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Using atomistic simulations we investigate the thermodynamical properties of a single atomic layer of hexagonal boron nitride (h-BN). The thermal induced ripples, heat capacity, and thermal lattice expansion of large scale h-BN sheets are determined and compared to those found for graphene (GE) for temperatures up to 1000 K. By analyzing the mean-square height fluctuations  $\langle h^2 \rangle$  and the height-height correlation function  $H(q)$  we found that the h-BN sheet is a less stiff material as compared to graphene. The bending rigidity of h-BN (i) is about 16% smaller than the one of GE at room temperature (300 K), and (ii) increases with temperature as in GE. The difference in stiffness between h-BN and GE results in unequal responses to external uniaxial and shear stress and different buckling transitions. In contrast to a GE sheet, the buckling transition of a h-BN sheet depends strongly on the direction of the applied compression. The molar heat capacity, thermal-expansion coefficient, and Grüneisen parameter are estimated to be  $25.2 \text{ J mol}^{-1} \text{ K}^{-1}$ ,  $7.2 \times 10^{-6} \text{ K}^{-1}$ , and 0.89, respectively.

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### I. INTRODUCTION

A single layer of hexagonal boron-nitride (h-BN) is a wide gap insulator that is very promising for optoelectronic technologies,<sup>1,2</sup> tunnel devices, and field-effect transistors.<sup>3-5</sup> According to the well-known Mermin-Wagner theorem,<sup>6</sup> the stability of any two-dimensional crystal is only possible in the presence of atomic corrugations which distort the perfect honeycomb lattice and allow the atoms to explore the out-of-plane direction. Experimental observations have found ripples in suspended sheets of graphene,<sup>7,8</sup> and atomistic simulations suggest that the strong bonds between the carbon atoms determine the features of these ripples.<sup>9</sup> Understanding the behavior of the ripples is important for many reasons.<sup>10</sup> They affect the electronic transport properties, e.g., in GE the ripples are believed to be one of the dominant scattering sources which limits the electron mobility.<sup>11,12</sup>

h-BN ribbons doped by carbon have recently been proposed.<sup>5,13</sup> In addition, BN based nanostructures are potential materials for thermal management applications<sup>14-19</sup> because of their high thermal conductivity and sensitivity to isotopic substitution, etc. Therefore, the knowledge of the shape and the temperature dependence of the intrinsic ripples is fundamental to devise novel nanodevices based on this material.

Both GE and h-BN sheets have a honeycomb lattice structure, however the different electronic properties and phonon band structure<sup>20-22</sup> result in unequal morphologies and corrugations. Transmission electron microscopy is widely used to resolve the individual atoms in suspended h-BN sheets<sup>23</sup> where ripples inherently exist. First-principle calculations have been performed using small unit cells, periodically replicated, which are unable to model long-wavelength corrugations which require thousands of atoms<sup>24</sup> while the mechanical properties of a h-BN sheet can be estimated by using discrete Fourier transform.<sup>25</sup> Conversely, atomistic simulations using molecular dynamics simulations (MD) enable us to study thermomechanical properties directly on large scale samples.

The modified Tersoff potential<sup>26</sup> (TP) (parametrized originally for carbon and silicon) with various sets of parameters have shown to predict reasonable values for the thermomechanical properties of the h-BN sheet. In the pioneer work by Albe *et al.*, reparametrized TP was used to study the impact of energetic boron and nitrogen atoms on a cubic-BN target.<sup>27</sup> Some other groups have also parametrized TP using various experimental data, e.g., Sekkal *et al.*<sup>28</sup> treated h-BN as a one-component system, using the same potential parameters for both boron (B) and nitrogen (N) (neglecting the B-N interaction) to investigate the structural properties. Matsunaga *et al.*<sup>29</sup> proposed the TP of B in order to simulate cubic boron carbonitrides which are compatible with the parameters of nitrogen fitted by Kroll,<sup>30</sup> and recently, Liao *et al.*<sup>31</sup> and Sevik *et al.*<sup>32</sup> reported TP parameters that were used to study the mechanical properties and the thermal conductivity of a h-BN sheet, respectively.

In this study, we investigate the thermal rippling behavior of free standing monolayer h-BN by using state-of-the-art molecular dynamics (MD) simulations. We adopted the TP potential reparametrized by Sevik *et al.* which has been shown to represent the experimental structure and the phonon dispersion of the two-dimensional h-BN sheet. We found that h-BN is more corrugated and a less stiff material as compared to GE. The height-height correlations can be explained by the theory for continuum membranes.<sup>33</sup> In addition, we report results of both uniaxial and shear stress of a h-BN sheet and compare it with those found for GE. The buckling transition for compressed h-BN occurs earlier than for GE and the induced pattern of ripples when subjected to either uniaxial or shear stress shows significant differences.

This paper is organized as follows. In Sec. II, we introduce the atomistic model and the simulation method. Then, in Sec. III we analyze the behavior of the thermal ripples of a h-BN sheet. Here, we obtain the bending rigidity, the heat capacity, the thermal-expansion coefficients, and we study the buckling transition of the h-BN sheet when uniaxial external strain and shear stress are applied. All the results are compared

with the ones obtained for a GE sheet. Finally, in Sec. IV, we present our conclusions.

## II. METHODS

Classical atomistic molecular dynamics (MD) simulation is employed to simulate large scale samples of h-BN and GE at temperatures varying from 10 K up to 1000 K. We used a modified Tersoff potential (which is an ordinary defined potential in the LAMMPS package<sup>34,35</sup>) according to the parameters proposed by Sevik *et al.* for the h-BN sheet. All the parameters and a detailed description of the potential energy is given in Ref. 32. To simulate GE we have used the AIREBO potential<sup>36</sup> which is suitable for simulating hydrocarbons. We employed  $N$ - $P$ - $T$  ensemble simulations with  $P = 0$  using the Nosé-Hoover thermostat which enables us to allow the size of the system to equilibrate (i.e., the size of the system is not fixed). All the reported values have been computed averaging over 300–400 snapshots taken over uncorrelated samples.

We start with a square-shaped h-BN sheet with periodic boundary conditions and initial dimensions  $322 \text{ \AA} \times 321 \text{ \AA}$  ( $315 \text{ \AA} \times 315 \text{ \AA}$  for GE) in the  $x$  and  $y$  direction, respectively, which correspond to a total number of  $N = 37888$  atoms, and which are sufficiently large in order to capture the long-wavelength regime. Periodic boundary conditions were adopted in both directions.

To analyze the thermal ripples we computed the diffraction pattern which is typically studied in experiments to detect the size and shape of the corrugations.<sup>7</sup> We obtained also the mean-square value of the out-of-plane displacements  $\langle h^2 \rangle$  of the atoms and, by following previous works,<sup>37,38</sup> the height-height correlation function  $\langle H(q) \rangle$  which was determined by considering an average of the height between the first neighbors of each atom. The latter was shown to follow a  $q^{-4}$  behavior that is expected from the theory of continuum two-dimensional membranes at large values of  $q$  in the harmonic approximation (see below). To analyze the differences between the strain induced corrugations in the h-BN and the GE sheets we applied uniaxial and shear stress on both systems as is schematically shown in Fig. 1. In order to apply strain we set the force on the two ends equal to zero and move the end atoms with an infinitesimal compression step ( $\delta x = 0.01 \text{ \AA}$ ) in the desired direction. After each compression step we wait for 2 ps to allow the system to relax and to ensure that the system is in thermal equilibrium.<sup>39</sup> Uniaxial compressive stress is applied along the zig-zag or armchair direction separately, and the shear stress is applied on the armchair edges with the opposite velocity for the top and bottom edges. The details of the used method of applying the boundary stress can be found in our previous studies.<sup>39–41</sup>

The TP function<sup>26</sup> used in the LAMMPS package<sup>34,35</sup> can be expressed as

$$E = \sum_i E_i = \frac{1}{2} \sum_{(i \neq j)} \phi(r_{ij}), \quad (1)$$

with

$$\phi(r_{ij}) = \sum_i \sum_{j(>i)} f_c(r_{ij}) [f_R(r_{ij}) + b_{ij} f_A(r_{ij})], \quad (2)$$

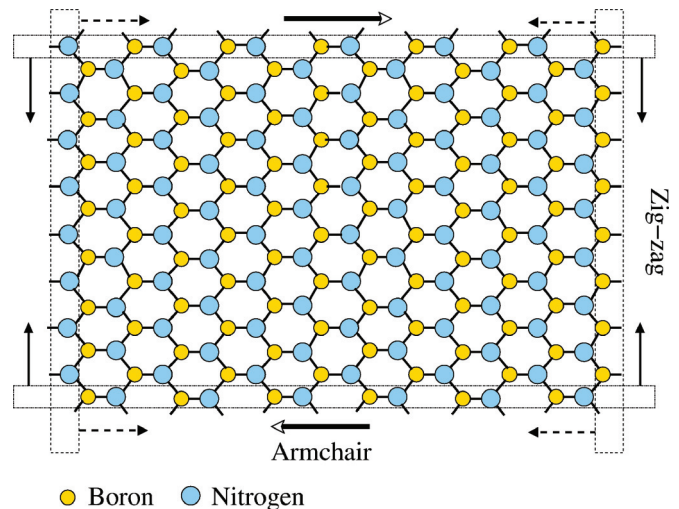


FIG. 1. (Color online) Schematic view of the single h-BN sheet. Smaller-yellow (bigger-blue) circles refer to the B (N) atoms. The rectangles indicate the atoms that are fixed during compression. Dashed (straight) lines correspond to armchair (zig-zag) uniaxial compression in the direction given by the arrows. Open arrows indicate the shear stress applied in the armchair direction.

where  $f_c$ ,  $f_R$ , and  $f_A$  are cutoff functions, the repulsive pair term, and the attractive pair term, respectively.  $r_{ij}$  and  $b_{ij}$  are respectively the distance from atom  $i$  to atom  $j$  and the bond order function. The use of TP disregard contributions coming from charge re-distribution which may occur in an ionic crystal. The inclusion of this effect in h-BN modifies the phonon spectrum significantly only for energies corresponding to the optical modes.<sup>42,43</sup> The large scale thermal ripples addressed here are governed mainly by the transversal acoustic mode (TA), which accounts for out-of-plane fluctuations, and it couples with the in-plane modes which renormalizes the long-wavelength behavior, e.g., the bending rigidity  $\kappa$  can be calculated directly from the TA mode.<sup>44</sup> Therefore, the charge redistribution is expected not to affect the thermal fluctuations analyzed here and the use of the TP is justified.<sup>45</sup>

## III. RESULTS AND DISCUSSION

### A. Thermal excited ripples

In Fig. 2(a) we show a height contour plot of the atoms of the h-BN sheet for an arbitrary snapshot taken during the MD simulation at 300 K. The corresponding modeled diffraction pattern is shown in Fig. 2(b). This pattern is very similar to the one obtained for the GE sheet<sup>7</sup> with the main difference in the distance between the Bragg points due to the unequal lattice constant of h-BN and GE. From the zoom plot around  $\mathbf{q} = (0,0)$  [Fig. 2(c)] one observes the local structure of the central Bragg point for these intrinsic thermal ripples of h-BN. Notice that the lack of the presence of the  $\mathbf{q} = (0,0)$  component is a consequence of the absence of a perfectly flat h-BN sheet.

The signatures of the thermal induced ripples can also be seen in the mean-square value of the out-of-plane fluctuations  $\langle h^2 \rangle$ . In Fig. 3(a) we show  $\langle h^2 \rangle$  as a function of temperature. In comparison with GE (included also in this figure for comparative purposes) we observe that  $\langle h^2 \rangle$  is always larger for

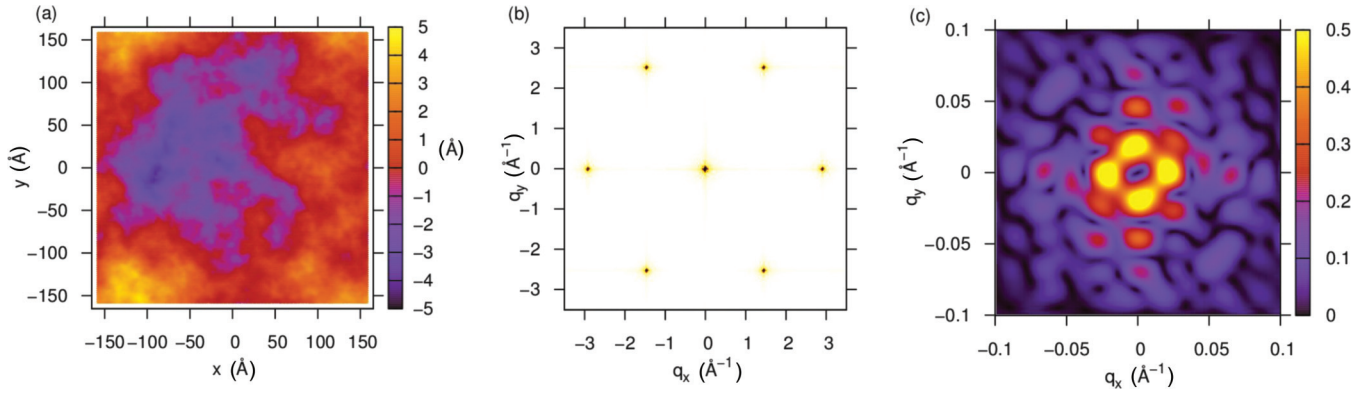


FIG. 2. (Color online) (a) Contour plot of the heights for an arbitrary snapshot taken during the MD simulation at 300 K. (b) Corresponding simulated diffraction pattern for the sample shown in (a). (c) Zoom view of (b) around  $\mathbf{q} = (0,0)$ .

the h-BN sheet. The weaker (stronger) the atomic B-N (C-C) bonds, the larger (smaller) the corrugations in h-BN (GE). Notice that the B-N bond is not pure covalent and it has an ionic character which is due to the different electronegativity between the two elements, i.e., the electrons are localized closer to the N atoms rather than the B atoms. Although this partially ionic structure of the h-BN layer increases the interlayer interaction resulting in a larger hardness of 3D bulk h-BN relative to graphite, it makes the single layer of BN less stiff than graphene. Moreover, the stacking of h-BN sheets in bulk h-BN is AAA stacking which is different for the ABC stacking in graphite.<sup>23</sup>

### B. Bending rigidity $\kappa$

According to the two-dimensional theory of continuum membranes the height-height correlation function, in the harmonic approximation, where the out-of-plane and in-plane

modes are decoupled, is expected to behave as

$$H(q) = \langle |h(q)|^2 \rangle = \frac{Nk_B T}{\kappa S_0 q^4}, \quad (3)$$

where  $\kappa$  is the bending rigidity of the membrane,  $N$  is the number of atoms of the sample,  $S_0$  is the surface area per atom, and  $k_B$  is the Boltzmann constant. In the large wavelength limit, i.e., for  $q \rightarrow 0$ , the height fluctuations are suppressed by anharmonic couplings between bending and stretching modes giving rise to a renormalized  $q$ -dependent bending rigidity and hence Eq. (3) is no longer valid.<sup>37,38,46</sup> In Fig. 3(b) we show  $\kappa$  for h-BN calculated from the harmonic part of  $H(q)$  between  $q = 0.5 \text{ \AA}^{-1}$  and  $q = 1 \text{ \AA}^{-1}$ . In agreement with the larger values of  $\langle h^2 \rangle$ , we observe that the h-BN membrane possesses a smaller  $\kappa$  as compared to GE and in the whole temperature range it is about 16% smaller at room temperature (300 K). Note that  $\kappa$  for both h-BN and GE increase with temperature. In Fig. 3(c) we show  $H(q)$  at 200 and 1000 K where the harmonic behavior can be clearly observed (fitted with a dashed line) and, as expected, with increasing temperature  $H(q)$  is shifted to larger  $q$ . This figure also reveals that the ripples are not characterized by a unique wavelength and instead follow the behavior expected from continuum membrane theory.

Before ending this section it is worthwhile to investigate an alternative method to estimate the bending rigidity (flexural rigidity). A common method for calculating the bending rigidity of the BN sheet is by performing simulations of BN nanotubes as a function of its radius ( $R$ ) of the curved tubes and then extrapolating the results to  $R \rightarrow \infty$ . Hence, one can calculate the elastic energy of the nanotube as a function of the inverse square of the radius,  $E = \frac{1}{2}\kappa R^{-2}$ . This method was used in Ref. 25 and in our previous work<sup>41</sup> to calculate the zero-temperature bending rigidity of GE and h-BN which were found to be 1.46 and 1.29 eV, respectively. The result obtained with the Tersoff potential using Eq. (3) is less than the result of Ref. 25. The bending rigidity of GE is larger than h-BN with about 0.15 eV in agreement with Ref. 25. In order to have an independent check we estimated the bending rigidity of a BN sheet by performing several ground-state simulations for  $(n,n)$  BN nanotubes with  $n = 5, \dots, 20$  using the Tersoff potential. Figure 4 shows the variation of the strain energy per atom as a function of the inverse square radius of the tube. Fitting a line to the data and dividing by the area of half of unit-cell atom

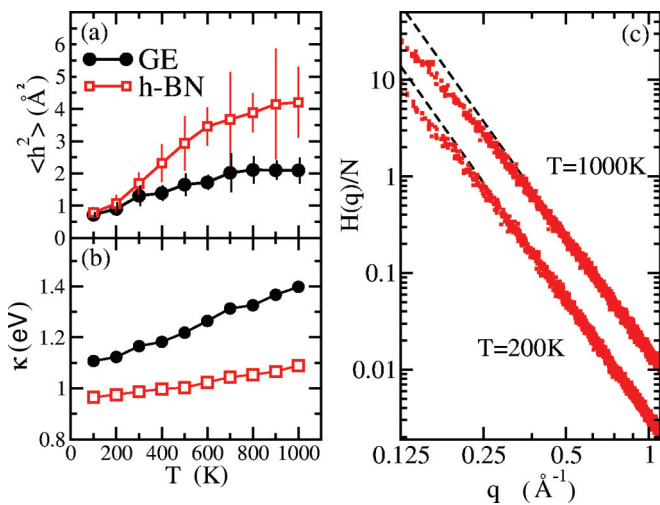


FIG. 3. (Color online) Variation of (a)  $\langle h^2 \rangle$  and (b) the bending rigidity versus temperature for both h-BN (open squares) and GE (solid circles). (c) Height-height correlation function  $H(q)$  of h-BN at two different temperatures is indicated. The dashed lines are the harmonic  $q^{-4}$  law.



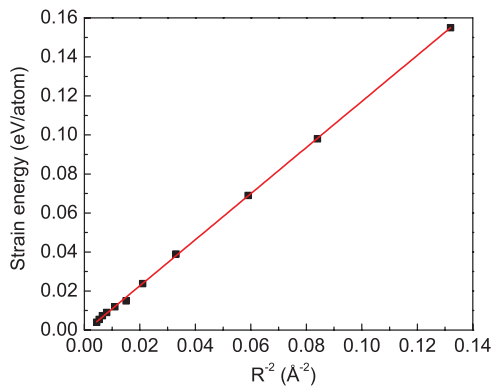


FIG. 4. (Color online) Variation of strain energy versus inverse square of BN-nanotube radius using Tersoff potential.

results in  $\kappa = 0.86$  eV. The result of the Tersoff potential agrees well with our estimation for  $\kappa$  using Eq. (3) (Ref. 25). Thus we can conclude that results based on the Tersoff potential underestimate the bending rigidity as compared to the result from DFT.

### C. Heat capacity, thermal expansion, and Gruneisen parameter

The variation of the total energy per atom with temperature ( $\geq 10$  K) is shown in Fig. 5(a). The total energy varies linearly with temperature and gives the corresponding lattice contribution to the molar heat capacity at constant pressure (the average size of the system after relaxation is taken constant) which for the h-BN sheet results into

$$C_P = \frac{dE_T}{dT} = 25.2(3) \text{ J mol}^{-1} \text{ K}^{-1}, \quad (4)$$

which is comparable to the one for a GE sheet, i.e.,  $24.5(9) \text{ J mol}^{-1} \text{ K}^{-1}$  and close to the well-known classical molar heat capacity, i.e.,  $C \simeq 24.94 \text{ J mol}^{-1} \text{ K}^{-1}$ , i.e., the Dulong-Petit value, where  $R$  is the universal gas constant. Notice that the heat capacity is a temperature-dependent parameter that will decrease for temperature below the Debye temperature. However, the classical MD simulation gives the correct high-temperature asymptotic limit, i.e., the Dulong-Petit value, but fails in the low and intermediate temperature range.

In Fig. 5(b) we show the variation of the averaged B-N bond length with temperature. The linear behavior enables us to

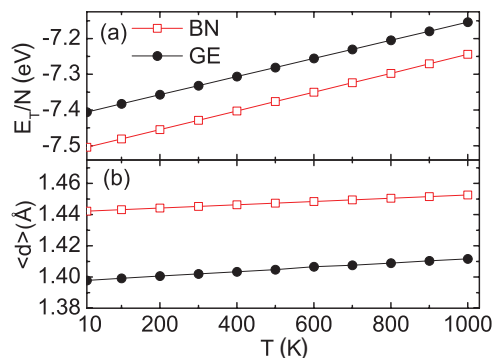


FIG. 5. (Color online) Variation of (a) the total energy per atom and (b) the averaged bond length versus temperature for h-BN and GE (the error bar is less than  $10^{-4}$  eV/atom for the total energy).

calculate the linear thermal expansion of the lattice parameter of a h-BN sheet as

$$\gamma_{\text{BN}} = \frac{1}{a} \frac{da}{dT} = 7.2(1) \times 10^{-6} \text{ K}^{-1}, \quad (5)$$

where  $a = 1.442 \text{ \AA}$  is the zero-temperature lattice parameter. The obtained  $\gamma$  is 33% larger than the one measured for cubic BN, i.e.,  $4.8 \times 10^{-6} \text{ K}^{-1}$ ,<sup>47</sup> and is comparable to the one found for GE, i.e.,  $\gamma_{\text{GE}} = 10.0(7) \times 10^{-6} \text{ K}^{-1}$ . The latter (i.e.,  $\gamma_{\text{GE}}$ ) is in good agreement with our previous studies.<sup>39,40</sup>

From the obtained values of  $\gamma$  and  $C$  we can compute the Gruneisen parameter,

$$\alpha_{\text{BN}} = \frac{\gamma B}{C\rho} = 0.89, \quad (6)$$

where  $B$  is the two-dimensional bulk modulus and  $\rho$  is the mass density. Using  $B_{h\text{-BN}} = 3 \text{ eV \AA}^{-2}$  [ $B_{\text{GE}} = 12.7 \text{ eV \AA}^{-2}$  (Ref. 48)],  $\rho_{h\text{-BN}} = 24.82/S_{h\text{-BN}} = 3.81 \times 10^{-4} \text{ g m}^{-2}$  ( $\rho_{\text{GE}} = 7.6 \times 10^{-4} \text{ g m}^{-2}$ ) for h-BN (GE), we obtain  $\alpha_{\text{BN}} = 0.89$  ( $\alpha_{\text{GE}} = 1.2$ ). Note that the estimated value of  $\alpha_{\text{GE}}$  is better than the one found in Ref. 49, i.e.,  $-0.2$ , and is closer to the experimental result, i.e.,  $2.0$ .<sup>50</sup>

### D. Buckling transition

The different stiffness between the h-BN and GE sheets results in different buckling transitions. To study this, we

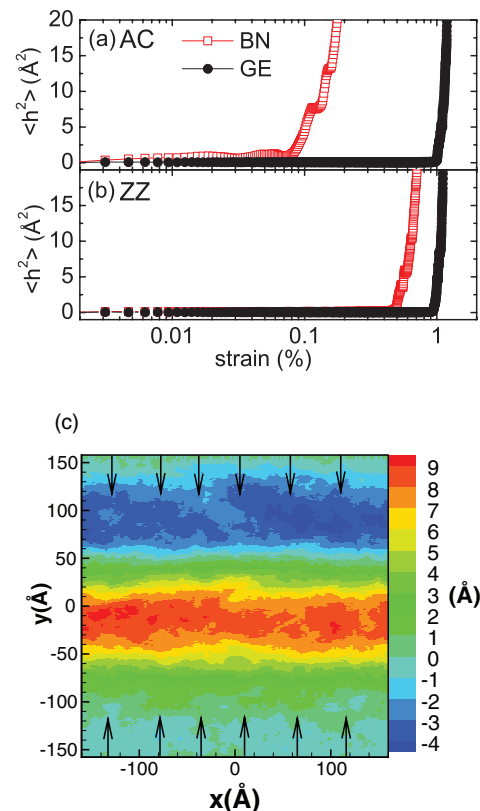


FIG. 6. (Color online) Variation of  $\langle h^2 \rangle$  versus external uniaxial strain in the (a) armchair and (b) zig-zag direction. Contour plot of the heights of compressed h-BN sheet samples subjected to a compressive strain for fixed  $\langle h^2 \rangle = 20 \text{ \AA}^2$  for compression in (c) zig-zag direction of the h-BN sheet. Arrows indicate the stress direction.

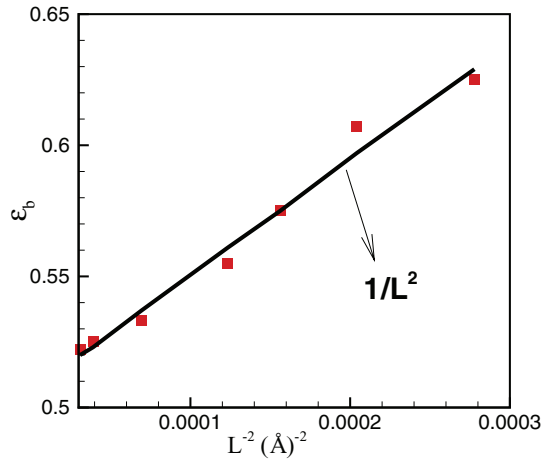


FIG. 7. (Color online) Variation of buckling strain with the longitudinal length of the BN sheet which is compressed along the zig-zag direction.

compressed the systems uniaxially where we considered both zig-zag and armchair directions. This was done by fixing one row of atoms in each edge during the compression steps as is indicated schematically in Fig. 1. The compression rate was taken  $\mu = 0.5$  m/s which is similar to the one used in our previous study,<sup>40</sup> and small enough to guarantee that the system is in equilibrium during the whole compression process.<sup>51</sup> The simulations were carried out at room temperature. Figure 6(a) shows the variation of  $\langle h^2 \rangle$  versus strain, i.e.,  $\epsilon = \mu t/l$  where  $t$  is the time (after starting the compression) and  $l$  is the initial box length in the direction of the compression. The buckling transition for the h-BN sheet kept at room temperature is found to be 0.6 (0.1) which is smaller than the one for GE, i.e., 1.0 (1.2), for uniaxial compression along the zig-zag (armchair) direction.<sup>52</sup> Hence, when the compression is applied in the zig-zag direction, the h-BN sheet resists much more against the external uniaxial stress as compared to the case where the stress is applied along the armchair direction. The smaller

critical strain at which the buckling transition in the armchair direction of the h-BN sheet takes place indicates its more sensitive nature to external uniaxial stress.<sup>53</sup> Although the same argument holds for GE, the difference between the two directions is much smaller. Notice that DFT calculations result in a deviation in bending rigidity (flexural rigidity) between ZZ BN-nanotube and AC BN-nanotube (ZZ becomes larger than AC) for radius smaller than  $\simeq 3$  Å,<sup>25</sup> while for larger radius they are the same.

A contour plot of the buckled h-BN sheet with  $\langle h^2 \rangle = 20$  Å<sup>2</sup> and compressed in the zig-zag direction is shown in Fig. 6(c). The obtained buckling transition for GE, i.e., 0.8%, agrees very well with our previous studies<sup>39</sup> and is in the range of the experimental measured buckling transition for suspended GE, i.e., 0.5–0.7%.<sup>54,55</sup>

It is also interesting to compare the buckling strain with those predicted by the theory of loaded beam. Euler theory for a two end-loaded beam having length  $L$  predicts that  $\epsilon_b \propto L^{-2}$ .<sup>40,56</sup> The first demonstration by MD of Euler buckling in nanostructures goes back to the pioneer work by Yakobson *et al.*<sup>57</sup> We performed several simulations in order to find the length dependence of the buckling strain for BN sheets which are, e.g., compressed along the zig-zag direction. Figure 7 shows the variation of  $\epsilon_b$  with the longitudinal length ( $L$ ) of the zig-zag BN sheet. The solid line is a fit to  $L^{-2}$  and the symbols are the results of our MD simulations which are qualitatively in agreement with the theory of loaded beam.

Finally, we report the results for h-BN and GE sheets under shear stress. Here we applied the stress only in the armchair direction as is described schematically in Fig. 1. We found that, due to the larger stiffness, to reach the same value of  $\langle h^2 \rangle$  a larger shear stress has to be applied in GE as compared to h-BN. In Figs. 8(a) and 8(b) one can observe significant differences between the corrugated configurations of h-BN and GE sheets. These samples were subjected to a shear stress of  $\epsilon = 1.5\%$ . While h-BN is highly sensitive to shear stress and deforms easily, GE can resist larger stress values due to its larger rigidity.

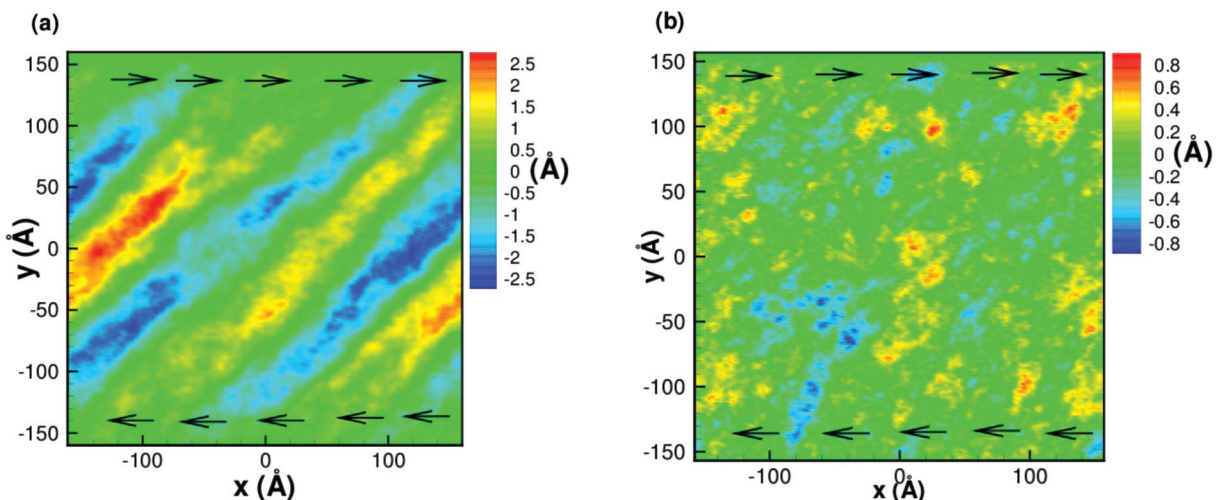


FIG. 8. (Color online) Effect of a shear stress of about 1.5% on the out-of-plane deformation of (a) the h-BN sheet and (b) the graphene sheet. Arrows indicate the stress direction on the armchair edges. Note the larger values of the heights in h-BN.

#### IV. CONCLUSIONS

The thermal properties of a boron nitride sheet were studied using large scale atomistic simulations. We showed that the scaling properties of a h-BN sheet follows closely the results of membrane theory and hence the thermal excited ripples are not characterized by any particular wavelength. Using the harmonic part of the height-height correlation function we found an increasing bending rigidity with temperature which is smaller than the one of graphene. We found that the buckling transition for h-BN depends on the applied compression direction and is much smaller than the one of graphene. The obtained molar heat capacity agrees very well with the well-known Dulong-Petit number,  $25.2 \text{ J mol}^{-1} \text{ K}^{-1}$  and the thermal-expansion coefficient was found to be positive and equal to  $7.2 \times 10^{-6} \text{ K}^{-1}$ . The Gruneisen parameter

0.89 is found to be smaller than the one for graphene, i.e., 1.2. We showed that the different stiffness between the GE and h-BN sheets leads to different patterns of deformations in the presence of either uniaxial or shear stress.

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