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Guidelines for passive control of traffic-related air pollution in street canyons: an overview for urban planning.

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Guidelines for passive control of traffic-related air pollution in street canyons: an overview for urban planning.

Abstract

1 Recent studies indicate the necessity of addressing traffic-related air pollution in urban
2 environments, as street canyons are known for their lack of natural ventilation and increased
3 pollution levels. To address this issue, numerous studies have been conducted on different aspects
4 (e.g. aspect ratio, orientation and height variation) and their impact on ventilation and pollution
5 dispersion/dilution performance in street canyons. Despite the numerous studies, the information
6 remains fragmented and the results and applications are fairly unknown in urban planning. Broad
7 review studies on numerous street canyon aspects are also quite scarce. In this study, over 200
8 studies were collected and reviewed across various parameters and on different configuration levels
9 (street canyon configuration / building configuration / in-canyon configuration). Hereby, the study
10 aims to give a comprehensive overview and to formulate spatial guidelines to improve the
11 application of the reviewed studies for the purpose of urban planning. In total, 19 general guidelines
12 were formulated, and an implementation strategy for the purpose of urban planning was developed.
13 Despite the usability of these guidelines for urban planning, a high number of limitations and
14 variabilities were detected. The broad literature review also revealed knowledge gaps, indicating the
15 potentials for further research.

Keywords

17 Urban design; Air pollution; Street canyon; CFD modelling

Nomenclature

ACH	air exchange rate	LEZ	low emission zones
AR	aspect ratio	PNC	particle number concentration
BHR	building height ratio	P_{vol}	pore volume
CFD	computational fluid dynamics	Re	Reynolds number
C_x	pressure loss coefficient	SF	skimming flow
H_d	building height of the downwind building	TMS	traffic management strategies
H_t	trunk height	V_d	deposition velocity
H_u	building height of the upwind building	V_{inlet}	inlet wind velocity
IRF	isolated roughness flow	WIR	wake interference flow
LAD	leaf area density	WOP	window opening percentage
LAR	lateral aspect ratio	Z_h	roof height
LBW	low Boundary Wall		

18 1. Introduction

19 According to the European Commission (2017) air pollution poses the second biggest environmental
20 concern for Europe after climate change. In urban environments, air pollution poses a high risk since
21 pollutants get trapped in the urban canopy layer (the layer of air extending from the ground surface
22 up to the level of the buildings) where human exposure to these pollutants is high. Vehicular
23 emissions are the predominant source of air pollution in the majority of urban environments
24 (Gallagher et al., 2015). In most urban environments, the urban canopy layer is defined by a high
25 number of street canyons (narrow inner urban roads, flanked by a continuous row of (high) buildings
26 on both sides), which promote the accumulations of traffic-induced pollution. Recent air quality
27 mappings in Europe (Paris (AIRPARIF, 2010), London (Environmental Research Group of Kings
28 College London, 2015) and Antwerp (Vito, 2019)) showed that the levels of air pollution (NO_2) in
29 street canyons are nearly as high as on highways and ring roads, although traffic intensity is lower.
30 This indicates that the lack of sufficient natural ventilation in street canyons plays an important role
31 in the accumulation of air pollution.

32 2. Problem statement

33 Since air pollution is recognized as an environmental threat, the EU has been working for
34 decades on the development of the EU's clean air policy, which is strongly focused on the reduction
35 of pollutant emissions. In most local policies, the actions are narrowed down to the reduction of the
36 impact of traffic on air quality by using traffic management strategies (TMS). As a result, air quality
37 action plans are applied with a strong emphasis on traffic regulations and policies that reduce private
38 car usage, stimulate public transport, traffic flow improvement, speed limit reduction, the
39 implementation of low emission zones (LEZs) and mobility plans (Panteliadis et al., 2014).
40 Scientific reviews in the last couple years on the efficiency of LEZs (Boogaard et al., 2012;
41 Panteliadis et al., 2014; Ezeah et al., 2015; Holman et al., 2015; Ku et al., 2020) all conclude
42 uncertain results. Boogaard et al. (2012) and Ku et al. (2020) indicate that local traffic policies,
43 including LEZs, are too modest to produce significant decreases in traffic-related air pollution.

44 Since the overall evidence of the effectiveness of TMS is weak (Bigazzi and Rouleau, 2017)
45 the improvement of air quality by implementing passive measures starts to gain more interest.
46 Passive control measures are mostly used to manipulate the natural ventilation patterns and hereby
47 enhance pollutant dispersion and reduce pedestrian exposure to air pollutants (Galagher et al., 2011).
48 This review study focusses mainly on spatial interventions which promote in-canyon ventilation and
49 thereby also promote pollutant dispersion. On a city-wide scale, numerous urban morphology
50 indices, such as gross floor area ratio, plan area density and frontal area density (summarized in
51 Badach et al., 2020) can be used to determine and improve the ventilation capacity of a city region.

52 However, on a local scale such as in street canyons, possible measures and their effect on
53 air quality are relatively unknown for urban planners. A high number of studies on different small-
54 scale measures to improve air quality in street canyons have been conducted, especially in the field

55 of engineering and bio-engineering. Moreover, this information remains fragmented, mostly
56 specified on one specific aspect and rather technical, which reduces the applicability for urban
57 planning. In order to support urban planners, this article aims to enumerate a number of potential
58 measures to improve air quality on a street canyon scale, supported by evidence (strong or weak)
59 from numerous studies. It should be stressed that, although a wide range of urban design measures
60 can be found, this research is narrowed down to the measures applicable to the small scale of the
61 street canyon which promote in-canyon ventilation and the dispersion of local traffic-related air
62 pollutants, since measures on this level are relatively unknown for urban planners.

63 3. Method

64 The method described in this article is derived from a method presented by Bigazzi and
65 Rouleau (2017), who performed a broad literature search to investigate the evidence on the
66 effectiveness of TMS. First, a number of design parameters were defined by using preliminary
67 research on the topic of urban design and the improvement of air quality on a local scale. These
68 fundamental preliminary works include researches conducted by Spirn (1986), Oke (1988), Theurer
69 (1999), Chan et al. (2001, 2003), Ng (2009, 2010), Garcia et al. (2013), Pijpers-van Esch (2015),
70 Krautheim et al. (2014), Yazid et al. (2014), Yuan et al. (2014), Lenzholzer (2015), Abhijith et al.
71 (2017) and Yang and Fu (2019). The selection of the first parameters were altered/extended during
72 the research process. In total, 12 parameters were selected, divided in three types of configuration:
73 Street canyon configuration with parameters:

- 74 • street canyon orientation
- 75 • aspect ratio
- 76 • street canyon depth
- 77 • street canyon length

78 Building configuration with parameters:

- 79 • building height variation
- 80 • building setback
- 81 • roof shape
- 82 • building permeability

83 In-canyon configuration with parameters

- 84 • semi-open settings
- 85 • trees
- 86 • hedges, low boundary walls and parked cars
- 87 • lane position

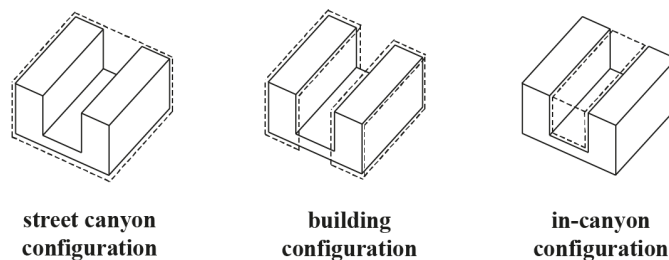


Figure 1. Overview of the reported configuration levels.

88 All parameters were submitted to the method of a scoping review (Xiao and Watson, 2017),
89 which aims to broadly and systematically search literature on every parameter. The information
90 extracted from the papers was compiled with the ambition to formulate overall conclusions for the
91 purpose of urban planning.

92 The scoping review was conducted using the EBSCO Discovery Service Database and Google
93 Scholar (<http://scholar.google.com/>). Based on the guidelines by Xiao and Watson (2017), search
94 strings with Boolean operators (“AND” and “OR”) were entered in the search engines. For each

95 parameter, a new search string was formulated with different synonyms. An example of such a
 96 search string in case of the parameter “aspect ratio” is: “street canyon” AND (“aspect ratio” OR
 97 “Height/Width ratio” OR “geometry”) AND (“air pollution” OR “flow regime” OR “pollutant
 98 dispersion”). The first and last term were kept the same for all parameters and the middle term was
 99 changed corresponding to the parameter. In case of a high number of relevant hits, the 20 most
 100 relevant studies were selected (first 20 hits of the database/search engine when ranked by relevance).
 101 However, for some parameters, the number of relevant studies did not exceed 20 or was fairly
 102 limited. An overview of all reviewed studies is represented in Table 1 and a more extensive overview
 103 incorporating the employed methods can be found in the **Appendix**. For each parameter, the main
 104 findings were summarized, and afterwards translated into specific guidelines for the purpose of
 105 urban planning and policy making. During the review process, a high number of variabilities and
 106 uncertainties (e.g. influence of surrounding urban morphology, impact of transboundary pollutants
 107 and other sources, impact of solar radiation and wall heating and chemical reactions between
 108 pollutants) were detected. These uncertainties are summarized in Section 5.2.

Table 1. Overview of the reviewed studies for every parameter.

Parameter	Number of studies reviewed	References
Street canyon orientation	20	Dabberdt and Hoydysh (1991), Oke (1997), Becker et al. (2002), Kim and Baik (2004), Brown et al. (2004), Pospisil et al. (2005), Voigtländer et al. (2006), Klein and Clark (2007), Soulhac et al. (2008), Xie et al. (2009), Hang et al. (2009), Soulhac and Salizzoni (2010), Afiq et al. (2012), Gromke and Ruck (2012), Yassin, M.F. (2013), Arkon and Özkol (2014), Zhang et al. (2016), Kwak et al. (2016), Niu et al. (2018), Huang et al. (2019a)
Aspect ratio	20	Hussain and Lee (1980), DePaul and Sheih (1985), Oke (1988), Hunter et al. (1992), Sini et al. (1996), Huang et al. (2000), Chan et al. (2001), Chan et al. (2002), Kovar-Panskus et al. (2002), Liu and Barth (2002), Walton and Cheng (2002), Caton et al. (2003), So et al. (2005), Bady et al. (2008), Wang and Mu (2010), Chung and Liu (2013), Yassin and Ohba (2013), Ngan and Lo (2016), Oke et al. (2017), Di Bernardino et al. (2018)
Street canyon depth	20	Lee and Park (1994), Sini et al. (1996), Baik et al. (1999), Chan et al. (2002), Kovar-Panskus et al. (2002), Liu et al. (2004), Li et al. (2008), Murena et al. (2008), Li et al. (2009), Wang and Mu (2010), Murena et al. (2011), Zhang et al. (2011), Murena (2012), Allegrini et al. (2013), Zhong et al. (2015), He et al., (2017), Zhong et al. (2017), Chew et al. (2018), Zhang et al. (2019), Zhang et al. (2020)
Street canyon length	15	Oke (1988), Hunter et al. (1990/1991), Hunter et al. (1992), Johnson and Hunter (1995), Kastner-Klein and Plate (1999), Chan et al. (2001), Chan et al. (2003), Kastner-Klein et al. (2004), Georgakis and Santamouris (2005), Hang et al. (2009), Ng (2010), Michioka et al. (2014), Yuan et al. (2014), Wang et al. (2017a), An et al. (2019)
Building height variation	20	Hoydysh and Dabberdt (1988), Baik et al. (1999), Gerdes and Olivari (1999), Sagrado et al. (2002), Assimakopoulos et al. (2003), Brown (2004), Xie et al. (2005), Xiamin et al. (2006), Gu et al. (2011), Zajic et al. (2011), Hang et al. (2012), Addepalli and Pardyjak (2013), Garcia et al. (2013), Miao et al. (2014), Nosek et al. (2016), Chen et al. (2017), Ming et al. (2018), Zhang et al. (2019), Park et al. (2020), Reiminger et al. (2020)
Building setback	8	Lne (2009), Ng and Chau (2014), Kanakiya et al. (2015), Huang et al. (2016b), Lau et al. (2017), Wen et al. (2017), Llaguna-Munitxa and Bou-Zeid (2018), Hassan et al. (2020)
Roof shape	20	Rafailidis and Schatzmann (1996), Rafailidis (1997), Louka et al. (1998), Kastner-Klein and Plate (1999), Theodoridis and Moussiopoulos (2000), Vlachogiannis et al. (2002), Xie et al. (2005), Huang et al. (2007), Huang et al. (2009), Yassin (2011), Kellnerova et al. (2012), Takano and Moonen (2013), Huang et al. (2015), King et al. (2015), Huang et al. (2016a), Llaguno-Munitxa et al. (2017), Llaguno-Munitxa and Bou-Zeid (2018), Wen and Malki-Epshtein (2018), Klukova et al. (2019), Nguyen et al. (2019)
Building permeability	20	Ng et al. (2006), Wong and Ng (2009), Ng and Chau (2011), Yuan et al. (2014), Ai and Mak (2015), Yang et al. (2015), Yang et al. (2016), Zhu (2016), Fan et al. (2017), Peng et al. (2017), Baghlad et al. (2018), Chew and Norford (2018), An et al. (2019), Gronemeier and Sühring (2019), van Druenen et al. (2019), Yang and Fu (2019), Zhang et al. (2019), Wong et al. (2020), Yang et al. (2020), Zhang et al. (2020)
Semi-open settings	20	Gerhardt and Kramer (1990), Hall et al. (2010), Kim et al. (2010), Hiyama et al. (2011), Hang et al. (2013), Hiyama et al. (2013),

		Montazeri and Blocken (2013), Lim et al. (2015), Marini et al. (2015), Sato et al. (2015), Murena and Mele (2016), Sahanavin et al. (2016), Suebyat and Pochai (2017), Hang et al., (2018), Llaguno-Munitxa and Bou-Zeid (2018), Weissert et al. (2018), Chomcheon et al. (2019), Ding et al. (2019), Pothipphan et al. (2019), Karkoulias et al. (2020)
Trees	20	Gromke and Ruck (2007), Buccolieri et al. (2009), Gromke and Ruck (2009), Buccolieri et al. (2011), Salim et al. (2011), Gromke and Ruck (2012), Ng and Chau (2012), Wania et al. (2012), Amorim et al. (2013), Li et al. (2013), Salmond et al. (2013), Abhijith and Gokhale (2015); Di Sabatino et al. (2015), Janhäll (2015), Jeanjean et al. (2016), Abhijith et al. (2017), Xue and Li (2017), Buccolieri et al. (2018), Huang et al. (2019b), Karttunen et al. (2020)
Hedges, low boundary walls and parked cars	18	McNabola et al. (2009), Keuken and Van Der Valk (2010), Gallagher et al. (2011), Wania et al. (2012), Vos et al. (2013), Abhijith and Gokhale (2015), Chen et al. (2015), Gallagher et al. (2015), Gromke et al. (2016), Lazzari et al. (2016), Li et al. (2016), Abhijith et al. (2017), Wang et al. (2017b), Kristof and Papp (2018), Baghlad et al. (2018), Kumar et al. (2019), Gallagher and Lago (2019), Ottosen and Kumar (2020)
Source position	6	Kastner-Klein and Plate (1999), Jicha et al. (2000), Chan et al. (2001), Liu and Barth (2002), Huang et al. (2015), Tan et al. (2019).

109 4. Results

110 The findings of the reviewed studies are hereafter described and summarized. In most
111 studies, wind/water tunnel modelling and CFD (computational fluid dynamics) have been used for
112 analyzing idealized street canyon configurations. It is important to bear in mind that the result of
113 these studies are abstractions from reality that merely aim to describe general effects of urban form
114 on airflow and pollution dilution and dispersion. They are intuitive ‘models’ helping researchers to
115 consider practical implications of different parameters. In some cases, simulations have been
116 supported with field studies, making the results more reliable. In general, it should still be stressed
117 that most results are strongly determined by site-specific arrangements, and a high number of
118 variables should be taken into account.

119 4.1 Street canyon configuration

120 Following aspects will be addressed within the scope of the street canyon configuration: street
121 canyon orientations (Section 4.1.1), aspect ratio (Section 4.1.2), street canyon depth (Section 4.1.3)
122 and street canyon length (Section 4.1.4). The main findings of every section are summarized in Fig.
123 2.

124 4.1.1 Street Canyon orientation

125 Despite the fact that in most cases street canyon orientation is fixed, it is important to
126 understand the correlation between the wind direction and its impact on natural ventilation and
127 pollutant accumulation. Based on the orientation of a street canyon, three flow patterns can be
128 distinguished: parallel, perpendicular or at an angle to the canyon’s axis (Afiq et al., 2012). A
129 comprehensive overview is illustrated in a recent study by Huang et al. (2019a), where a CFD study
130 of an idealized street canyon with $L/H = 10$ and $W/H = 1$ was subjected to seven different wind
131 directions ($\Theta = 0^\circ, 15^\circ, 30^\circ, 45^\circ, 60^\circ, 75^\circ$ and 90°). For parallel or nearly parallel wind directions
132 ($\Theta = 0^\circ, 15^\circ$) the model showed that the flow is mainly governed by a street-axis flow. When the
133 angle increased to 30° and 45° , a corkscrew like flow appeared and for $\Theta = 60^\circ$ and 75° a corkscrew
134 like flow appeared in the upwind part of the street canyon while the downstream part was
135 characterized by a clockwise vortex structure. Once $\Theta=90^\circ$ (perpendicular), the clockwise vortex
136 structure was developed in the entire street canyon. The same wind patterns were found in earlier
137 studies by Oke (1997), Soulhac et al. (2008) and Pospisil et al. (2005). A CFD study by Hang et al.
138 (2009), which assumed parallel wind directions, indicates that at a distance of about $6H$ (for a canyon
139 with $W/H = 1$, $W =$ width and $H =$ height) the velocity becomes nearly constant and does therefore

140 not increase or decrease further. The higher the W/H ratio, the further into the street canyon this
141 fully developed flow starts.

142 Regarding pollutant dispersion patterns, studies by Dabberdt and Hoydysh (1991), Xie et al.
143 al. (2009), Yassin (2013), Zhang et al. (2016), Huang et al. (2019a) and field studies by Voigtländer
144 et al. (2006), Arkon and Özkol (2014) and Kwak et al. (2016) all conclude that the highest
145 concentration occurs at the leeward oriented wall in case of oblique or perpendicular wind directions.
146 However, the difference in concentration levels between both sides of the street canyons does not
147 hold in case of parallel winds ($\Theta = 0^\circ$). Regarding longitudinal and lateral pollutant dispersion, a
148 wind tunnel study by Gromke and Ruck (2012) and a CFD study by Huang et al. (2019a) showed
149 that for perpendicular winds (lateral dispersion), a decrease in pollutant levels near the wall ends
150 was found, whereas for oblique and parallel winds (longitudinal dispersion) the pollutant levels
151 increased towards the downwind street canyon end. The same peak at the street canyon end in case
152 of parallel winds was found in a field study by Niu et al. (2018). The main findings of previously
153 indicated studies are summarized in Fig. 2. It should be stressed that these findings do not hold for
154 every situation. In some cases, concentration levels in case of parallel winds (due to the mean
155 advection along its axis) or oblique winds (due complex urban configurations or the presence of
156 trees) can exceed the pollution levels compared to perpendicular winds (Soulhac and Salizzoni,
157 2010; Niu et al., 2018; Gromke and Ruck, 2012). Conclusion from the Joint Urban 2003 Tracer
158 Experiment (Brown et al., 2004 and Klein and Clark, 2007) and an early field study by Johnson and
159 Hunter (1999) also showed that small variations of wind direction can significantly change in-
160 canyon flow properties and in-canyon wind direction can rapidly shift by 120-180°. Brown et al.
161 (2004) found typical along-canyon flow motions, even for wind directions perpendicular to the street
162 canyons. Detailed flow studies by Becker et al. (2002) and Kim and Baik (2004) also observed far
163 more complex 3D flow fields (Fig. 7) than those represented in Fig. 2.

164 Regarding urban planning, it can be concluded that street canyons are preferably oriented
165 parallel to the prevailing wind direction, provided that their length stays limited ($LAR < 12$, see
166 Section 4.1.4). However, the orientation of a street canyon is not adjustable in an existing urban
167 fabric. Still, the knowledge on street canyon orientation helps understanding the potentials of street
168 canyons with an orientation parallel to the prevailing wind direction, since they have the ability to
169 supply fresh air deep into the urban fabric when obstacles are limited (Ng, 2010; Quintiens, 2017).

170 4.1.2 Aspect ratio

171 Numerous studies have been conducted on the relationship between the ratio of the building
172 height to the street width (H/W ratio), also known as the aspect ratio (AR), and the impact on the
173 flow field and pollution dispersion. Early research by Hussain and Lee (1980), DePaul and Sheih
174 (1985), Oke (1988) and Sini et al. (1996) gives fundamental insight on the development of three
175 typical flow regimes and their threshold AR values for street canyons subjected to the boundary
176 condition of perpendicular approach flows: (1) an isolated roughness flow (IRF) appears when
177 buildings are widely spaced ($AR < 0.35$), (2) a wake interference flow (WIF) arises when the 0.35
178 $< AR < 0.65$ and (3) a skimming flow (SF) appears when $AR > 0.65$. Oke (1988) describes that the
179 transition between the three regimes is defined by the critical combination of the AR and the L/H
180 ratio (where L is the length of the continuous facade of the street canyon) or lateral aspect ratio
181 (LAR). When the LAR increases, skimming flow can occur with lower ARs. Corresponding results
182 were found by Chan et al. (2002), Kovar-Panskus et al. (2002) and Ngan and Lo (2016). An early
183 study by Hunter et al. (1992) also indicated the presence of corner eddies (recirculation zones) near
184 the corners of the leeward facade of the street canyon, changing the flow regimes. In this case, the
185 transition to WIF will only occur for canyons sufficiently wide so that the corner recirculation zones
186 fully formed. However, a field study by Johnson and Hunter (1999) showed that in a street canyon
187 with $AR = 0.4$, where a WIF or IRF is expected, a SF was present. The study therefore suggests that
188 factors additional to relative canyon geometry are relevant in determining flow regimes.

189 Caton et al. (2003) and So et al. (2005) stress the impact of the incoming flow
190 characteristics. They conclude that the development of a specific flow regime is closely related to
191 the turbulence of the incoming flow, defined by the Reynolds number (Re). In most reduced scale
192 studies (wind and water tunnel or CFD), Re varies between 400 (So et al., 2005) and 2.1×10^6
193 (Yassin and Ohba, 2013) and in case of full-scale studies (mostly CFD) Re varies between $1.10 \times$
194 10^5 (Chung and Liu, 2013) and 5.0×10^7 (He et al., 2017). A full list of the retrieved Re values for
195 the reviewed studies can be found in the **Appendix**. In reality, atmospheric flows tend to be highly
196 turbulent, and a large Re (an order of magnitude up to 10^6) should be taken into account (Lee and
197 Park, 1994; Zajic et al., 2011; Zhang et al., 2011; He et al., 2017; Zhang et al., 2020). Chew et al.
198 (2018) found that depending on the aspect ratio, the development of the different flow regimes
199 requires different limit Reynolds numbers to be exceeded.

200 The levels of air pollution are closely related to the flow regimes. Numerous studies (Huang
201 et al., 2000; Chan et al., 2001; Liu and Barth, 2002; Bady et al., 2008; Wang and Mu, 2010, Yassin
202 and Ohba, 2013 and Di Bernardino et al., 2018) show lower pollution levels in wide street canyons
203 (IRF, WIF) compared to narrow street canyons (SF). These studies suggest that canyon geometry
204 should be restricted to threshold values for SF. Chung and Liu (2013) indicate $AR = 0.5$ as a
205 threshold value for pollutant removal and indicate a sharp reduction of the pollutant exchange rate
206 once $AR > 0.5$. When considering in-canyon pollutant dispersion in case of a SF and perpendicular
207 wind, numerous studies (Huang et al., 2000; Chan et al., 2001; Walton and Cheng: 2002; Wang and
208 Lu, 2010, Yassin and Ohba, 2013, Di Bernardino et al., 2018) indicate increase pollution levels (2-
209 3 times higher) on the leeward facade.

210 Previously described studies have the potential to support the formulation of guidelines for
211 urban planning, such as the restriction of the AR to the threshold values for SF ($AR < 0.65$ (Oke,
212 1988) or $AR < 0.5$ (Chung and Liu, 2013)). However, as Oke (2017) already states, most studies
213 merely represent an abstraction from reality. Numerous impact factors should be taken into account
214 such as wind turbulence (Caton et al., 2003 and So et al., 2005), background pollution and pollution
215 source strength. A field study by Miao et al. (2020), for example, showed lower pollution
216 concentrations in narrow street canyons compared to wide street canyons, likely related to the lower
217 amounts of traffic in the narrow street canyons. Brown (2004) indicates that it may also be hard the
218 find a case where these simple vortex flows exist, since the flow field will most likely be a complex
219 combination of 2D and 3D vortices and channelized flow.

220 *4.1.3 Street Canyon depth*

221 The canyon depth is closely related to the aspect ratio (AR). A street canyon is defined as
222 deep once $AR > 1.5-2.0$ (Murena et al., 2008; Vardoulakis et al., 2003). In this case, deviating flow
223 patterns and enhanced pollutant concentrations can be expected (Vardoulakis et al., 2003). In most
224 studies, deep street canyons promote the development of two counter-rotating vortices, with the
225 bottom vortex weaker than the upper one (Murena, 2012). However, the threshold AR values for the
226 development of the two vortices vary in different studies. Studies by Sini et al. (1996), Baik et al.
227 (1999), Kovar-Panskus et al. (2002) and Chan et al. (2002) show two in-canyon vortices once $AR >$
228 $1.43-1.65$. Additional studies by Murena (2012) and Li et al. (2008) even report 3 vortices once AR
229 > 3.0 (also found by Sini et al., 1996). In very deep street canyons with $AR=10$, 8 vortices were
230 reported by Li et al. (2009).

231 When comparing different studies, it can be concluded that the appearance of these flow
232 regimes strongly depends on two main aspects: wind speed and turbulence levels. In case of lower
233 wind speeds ($V_{inlet} = 2-3 \text{ m s}^{-1}$) or lower turbulence values ($Re < 2.5 \times 10^6$ in case of full-scale studies),
234 a double vortex was reported for $AR = 1-2.7$ (Lee and Park, 1994; Chang et al., 2002; Allegrini et
235 al., 2013; Zhang et al., 2019). In case of higher wind speeds (15 m s^{-1}) or higher Re values ($\approx 5 \times 10^6$
236 in case of full-scale studies) no double vortex structure was found for $AR = 1 - 4$ (Chang et al.,
237 2002; Zhang et al., 2011, 2019, 2020). Only when $AR > 5$, a double vortex was developed. A field
238 campaign by Eliasson et al. (2006) in a street canyon with $AR \approx 2,1$ also reported that no evidence
239 could be found for the existence of a double staggered vortex in case of perpendicular winds.

240 Once a secondary vortex is formed, pollution levels are strongly enhanced and the highest
241 pollution level shifts to the windward facade instead of the leeward facade (Liu et al., 2004; Zhong
242 et al., 2015; Zhong et al., 2017; Zhang et al., 2019; Zhang et al., 2020). The sharp increase in
243 pollutant levels can be explained by the strongly reduced wind speed (Kovar-Pankus et al., 2002),
244 low mass transfer velocity (Murena et al., 2011) and high retention value (Wang and Mu, 2010)
245 when a secondary vortex is formed. Due the low wind speed, the difference in pollution levels
246 between the windward and leeward facade is also less distinguished than in case of a single vortex
247 (Murena et al., 2008; Li et al., 2009).

248 Related to urban design it can be concluded that the potential development of a secondary vortex
249 should be avoided. First of all, $AR = 5$ should be respected as an upper bound for a street canyon
250 AR (Li et al., 2009). For street canyons with an AR ranging from 1-5, wind speed and turbulence
251 should be taken into account to predict the development of a secondary vortex. Zhang et al. (2020)
252 investigated the impact of wind catchers and concluded that wind catchers have the potential to
253 destroy multi-vortex flow patterns, produce single-vortex structures and hereby enhance street
254 ventilation capacity, which could lead to a significant pollutant reduction by an order of magnitude
255 up to two. However, it should be born in mind that the actual vortex formation in deep street canyons
256 is still largely unpredictable.

257 4.1.4 *Street Canyon length*

258 As described in section 4.1.2, Oke (1988) introduced the importance of the length of the
259 street canyon, where the lateral aspect ratio (LAR) influences the appearance of different flow
260 regimes. Only a few years later, Hunter et al. (1990/1991) conducted further research on this matter
261 and classified street canyons with $LAR < 3$ as short, $LAR = 5$ as medium and $LAR > 7$ as long. In
262 accordance to Oke (1988), they concluded that in case of long street canyons, skimming flow could
263 occur in case of lower ARs. In 1992, Hunter et al. investigated the development of corner eddies
264 (also called lateral recirculation zone; Kastner-Klein et al., 2004) near the street canyon's outer ends.
265 An experimental study by Kastner-Klein et al. (2004) and a CFD study by Michioka et al. (2014)
266 show that for short street canyons ($LAR < 4$) under perpendicular wind conditions, the lateral
267 recirculation zones converge in the center of the street canyon, causing strong vertical motions which
268 promote ventilation and pollutant reduction. When LAR increases (> 4), the impact of the corner
269 recirculation reduces in the middle section of the street canyon, and pollutant accumulation is
270 promoted in this area (Hunter et al., 1992; Johnson and Hunter, 1995; Kastner-Klein and Plate, 1999;
271 Chan et al., 2001; Kastner-Klein, 2004).

272 In case of parallel winds, long street canyons can operate as air paths, supplying fresh air
273 in the urban fabric (Ng, 2010). A CFD study Hang et al. (2009) shows that the maximum wind speed
274 in a street canyon under parallel wind conditions increases sharply from $LAR = 4$ -12 and then levels
275 off. This indicates that in long street canyons ($LAR > 12$), wind speed is more likely to decrease
276 resulting in pollutant accumulation at the end of the street canyon.

277 With regard to urban design, it can be concluded that long street canyons are preferably
278 oriented parallel to the dominant wind direction (Ng, 2010; Wang et al., 2017a). However,
279 channelized winds can be strong and result in an unpleasant pedestrian environment (Lenzholzer,
280 2015). When oriented perpendicularly, $LAR = 4$ can be used as a threshold value (Chan et al., 2001;
281 Georgakis and Santamouris, 2005; Michioka et al., 2014). Michioka et al. (2014) indicate that the
282 aforementioned effects only take place in case of simplified models. Once the complexity of the
283 model increases, more complex wind fields occur and irregularities in pollutant dispersion are
284 notable.

285 Street canyon lengths can be limited by introducing intersections and increasing building
286 permeability. A more complex CFD study by Yuan et al. (2014) showed reductions up to 25 % of
287 the average normalized concentration in the mean street when the overall permeability of the street
288 was increased by ≈ 30 %. Another complex CFD model by An et al. (2019) illustrated that the
289 introduction of a single building separation in the middle of a street canyon could locally decrease
290 air pollution levels by 80 %. Despite the promising results, no field studies were conducted on this

291 matter. Even more, none of these studies considered the impact of intersections on traffic flow and
 292 traffic congestions. Therefore, conclusions should be carefully considered. The main findings of the
 293 effects of the street canyon configuration (Sections 4.1.1 – 4.1.4) on the in-canyon flow field and
 294 pollutant distribution are summarized in Fig. 2.

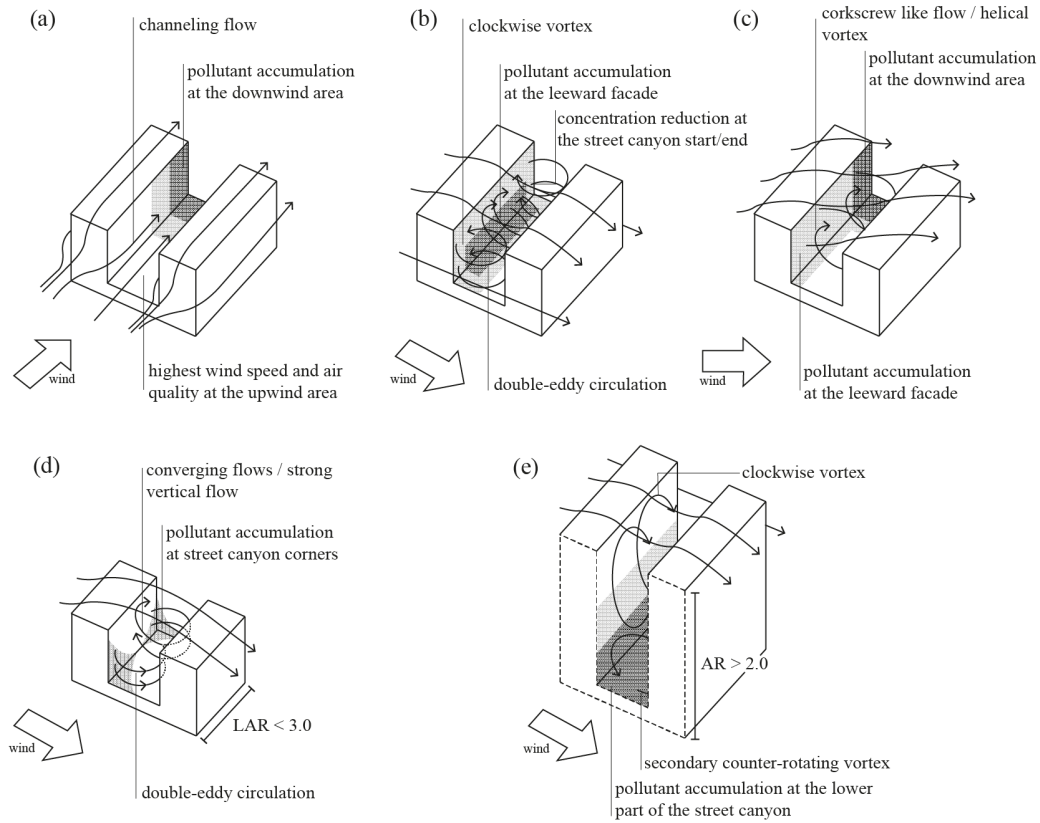


Figure 2. Estimated flow regimes and pollutant distribution for: (a,b,c) different orientations of the street canyon towards the prevailing wind direction, (d) short street canyons (LAR < 3.0) with converging flows and (e) deep street canyons (AR > 2.0) with a double vortex structure. Modified after Johnson and Hunter (1995), Oke (1997), Huang et al. (2019a), Soulhac and Salizzoni (2010), Michioka et al. (2014), Pijpers-van Esch (2015) and Zhang et al. (2019, 2020).

295 4.2 Building configuration

296 4.2.1 Building height variation

297 In general, it is assumed that changes in building height have the potential to enhance or
 298 reduce ventilation in street canyons. In most studies, the variance in building height is expressed by
 299 the ratio between the height of the upwind building (H_u) and the height of the downwind building
 300 (H_d), also called the building height ratio (BHR; Zajic et al., 2011). Street canyons are generally
 301 called step-down street canyons when BHR > 1 (upwind building is higher than the downwind
 302 building) and step-up canyons when BHR < 1 (upwind building is lower than the downwind
 303 building). Based on multiple studies (Hoydysh and Dabberdt, 1988; Gerdes and Olivari, 1998;
 304 Sagrado et al., 2002; Assimakopoulos et al., 2003; Xie et al., 2005; Ming et al., 2018) it can be
 305 assumed that in most cases, pollution levels tend to be higher in step-down canyons compared to
 306 step-up street canyons.

307 The lower pollutant levels in step-up street canyons can be explained by the so called
 308 ‘downwash’ effect. This phenomenon is caused by the flow blockage in front of the higher
 309 downwind building, which enhances the strength of the downdraft flow near the windward facade
 310 of the downwind building resulting in divergent flow in the lower part of the street canyon (Miao et

311 al., 2014). These divergent flows enhance pollutant dilution to the leeward facade and due to the
 312 low building height of the leeward building, pollutants are transported rapidly to the roof level and
 313 afterwards diluted by the wind (Ming et al., 2018). For most idealized cases (with $AR \approx 1$, where AR
 314 is defined by the ratio between the height of the upwind building (H_u) and the street width) with
 315 perpendicular winds, it is assumed that a downwash effect is created once $BHR < 0.8$ (Xie et al.,
 316 2005; Miao et al., 2014; Ming et al., 2018).

317 In case of step-down street canyons, Assimakopoulos et al. (2003) showed that in an
 318 idealized street canyon with $AR = 1$ and $BHR = 2$, pollutant levels in the lower corner of the
 319 downwind building increase by $\approx 30\%$ and in the lower corner of the upwind building by $\approx 300\%$
 320 compared to the concentration levels in an even street canyon ($AR = 1$ and $BHR = 1$). Visualizations
 321 by Baik et al. (1999), Xie et al (2005), Xiaomin et al. (2006) and Reiminger et al. (2020) show a
 322 single vortex in case of a step-up canyon ($AR = 0.5$ and $AR = 1$) and in case of a step-down canyon,
 323 the main clockwise vortex shifts above the downwind building roof and a secondary
 324 counterclockwise vortex is formed in the lower region of the street canyon (Fig. 3). Therefore, higher
 325 pollutant levels are found at the windward facade in case of a step-down configuration (Xie et al.,
 326 2005). Despite the overall agreement that step-down street canyons are less favorable in terms of air
 327 quality and ventilation, Miao et al. (2014) concluded that a step-down setup can potentially results
 328 in improved ventilation due the formation of the large recirculation clockwise vortex at the leeward
 329 facade of the higher building and divergent flows in the lower part of the street canyon.

330 It also seems that in case of longer (L/W -ratio > 3.0) or deeper ($AR > 2$) street canyons, the
 331 effect of the BHR becomes less distinguished (Assimakopoulos et al., 2003; Addepalli and Pardyjak,
 332 2013; Park et al., 2020). A CFD study by Zhang et al. (2019) even indicates that for very deep street
 333 canyons ($AR = 5$), a step-up notch ($BHR = 0.83$) can potentially create a third rotating vortex,
 334 resulting in a decreased pollutant dilution capacity.

335 It should be noted that in most of the aforementioned studies, the building heights is only
 336 changed for the entire length of a building, which in most cases is not a suitable configuration to
 337 represent real urban environments. Gu et al. (2011) and Nosek et al. (2016) investigated more
 338 complex 3D CFD models with an uneven and non-uniform building layout. Gu et al. (2011) found
 339 that pollution levels are in general lower in non-uniform street canyons than in even street canyons,
 340 and Nosek et al. (2016) also reported lower pollution levels in averaged step-up canyons but higher
 341 pollutant levels in averaged step-down canyons. The study of Gu et al. (2011) also showed that
 342 separate or isolated notches have a potentially larger impact on the reduction of in-canyon air
 343 pollutants, where adjoining notches have less impact. In most studies, the building height variability
 344 is also limited ($0.33 < BHR < 2.0$). Therefore, the effect of high-rise buildings is not taken into
 345 account. On a larger scale, Hang et al. (2012), Garcia et al. (2013), Chen et al. (2017) and Yang and
 346 Fu (2019) indicate that selective high-rise buildings might be interesting to improve air quality in
 347 street canyons, especially on the downwind side of the street canyon.

348 Related to urban planning, it can be concluded that building height variation can largely
 349 affect in-canyon flow patterns. In general, street canyons with a higher building height variation
 350 tend to create more turbulence, resulting in an increased in-canyon ventilation. Therefore, the classic
 351 street-canyon configuration with homogeneous building heights should be reconsidered. When
 352 introducing building height variations, the orientation towards the main wind direction should be
 353 kept in mind, where step-down configurations seem to worsen in-canyon ventilation and step-up
 354 configurations tend to improve in-canyon ventilation. However, further research should still be
 355 conducted on this matter.

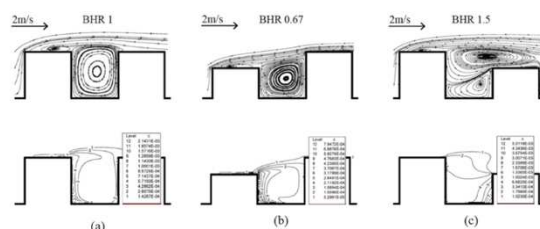


Figure 3. Estimated streamlines and concentration profiles for (a) even street canyons, (b) step-up street canyons and (c) step-down street canyons. Modified after Xie et al. (2005).

357 Whereas previous indicators are relatively well investigated, the impact of building
358 setbacks has received less attention. Only eight relevant articles/studies could be found within the
359 literature search. Ng and Chau (2014) conducted a broad research on the matter using a CFD
360 simulation with horizontal (full length) and vertical (full height) setback configurations (see Fig 4).
361 According to Ng and Chau (2014) building setbacks can be beneficial for personal exposure to air
362 pollution in case of perpendicular winds. However, their efficiency largely depends on the aspect
363 ratio (AR) of the street canyon. A study by Ng and Chau (2014) showed that in case of regular street
364 canyons ($AR < 2$), a full-height vertical setback could induce higher flow velocities in the upper part
365 of the canyon together with the formation of a large counter-rotating vortex formed in the vertical
366 setback, which reduced in-canyon pollutants and increased the air exchange rate (ACH) at the top
367 of the street canyon. In contrast, horizontal setbacks resulted in a lower flow velocity. On the other
368 hand, full-length horizontal setbacks seemed to disrupt the vortex structure in deep street canyons
369 ($AR = 4-6$), resulting in increased flow velocities at pedestrian levels. In this case, the pollutant levels
370 at pedestrian level are reduced and the ACH at the top of the street canyon increased. The same
371 conclusions for full-length horizontal setbacks were made by Wen et al. (2017). Other studies
372 indicating the potential effect of building setbacks on improving in-canyon ventilation were
373 conducted by Kanakiya et al. (2015), Huang et al. (2016b), Lau et al. (2017) and Hassan et al. (2020)
374 which recommend full-length horizontal setback in case of a deep street canyon under perpendicular
375 winds, and a study by Ise (2009) which illustrates the potential of full height vertical setback
376 at the downwind side of the street canyon (with a potential reduction of 10 % for PM₁₀ and 25 %
377 for NO₂). A horizontal setback can not only be implemented at ground level, but also at roof level
378 (also called upper void podium; Hassan et al., 2020). Studies by Hassan et al. (2020) and Llaguna-
379 Munitxa and Bou-Zeid (2018) indicate that an upper void setback can also promote the vertical
380 transport of pollutants. However, the results also show that the pollutant reduction at pedestrian level
381 is rather limited, but the overall in-canyon pollutant level can be reduced by almost 50 %. Horizontal
382 setbacks on different heights have not been investigated yet. However, Spirm (1986) and Ng. (2009,
383 2010) suggest that a stepped street canyon profile improves ventilation and reduces air pollution.

384 In case of a parallel prevailing wind direction, Spirm (1986) and Ng and Chau (2014) state
385 that it is not recommended to use setbacks as this will possibly result in higher personal exposures
386 compared to street canyons without setback (estimated pollutant increase by 168 % up to 272 %; Ng
387 and Chau, 2014).

388 Regarding to urban planning it can be concluded that the type of setback should be
389 considered based on the AR and the prevailing wind direction. However, due the lack of sufficient
390 studies (e.g. studies on different wind directions or field studies), the introduction of building
391 setbacks as a potential solution for air pollution should be carefully considered, and location-specific
392 studies should be conducted in advance.

393 *4.2.3 Roof Shape*

394 The impact of different roof shapes (flat, slanted (or pitched or gable), wedged, trapezoidal and
395 vaulted) on flow patterns and pollutant dilution has widely been researched. CFD studies by
396 Theodoridis and Moussiopoulos (2000) and Wen and Malki-Epshtein (2018) indicate that due to the
397 presence of slanted roof, a weak counter-rotating vortex is created in the lower part of the canyon,
398 resulting in a decreased ventilation capacity. On the other hand, multiple other studies by Rafailidis
399 (1997), Louka et al. (1998), Vlachogiannis et al. (2002), Abdulsahab and Kumar (2010), Kellnerova
400 et al. (2012), King et al. (2015), Garau et al. (2018), Llaguno-Munitxa and Bou-Zeid (2018) indicate
401 improved ventilation and reduced pollutant levels in case of slanted roofs. These studies indicate
402 that pitched roofs improve pollutant dispersal due to the enlargement of the vortices penetrating into
403 the street canyon, aiding the in-canyon ventilation and reducing pollutant accumulation. It is also
404 thought that different non-flat roof typologies increase turbulence, improving pollutant dilution
405 (Llaguno-Munitxa et al., 2017). The discussion of whether non-flat roof typologies increase or

406 decrease urban ventilation can mostly be reduced to whether or not a double or single vortex
407 structure appears. However, the discrepancy between previous studies on this matter suggests the
408 impact of different parameters such as aspect ratio, roof height, roof shape and roof slope.

409 CFD studies by Huang et al. (2007, 2009, 2015, 2016a), Nguyen et al. (2019) and Yassin
410 (2011) suggest that the appearance of a single or double vortex structure largely depends on the roof
411 shape and the roof height. The results of the more favorable and unfavorable configurations in terms
412 of street canyon ventilation are summarized in figure 4. In general, it is thought that the lowest
413 pollution level occurs in the canyon with the downward wedged roof. However, Takano and Moonen
414 (2013) suggest that the beneficial effect depends on the roof slope, and critical slope of $\approx 18^\circ$ (for a
415 street canyon with $AR = 1$) was found to be the switching point between double and single vortex
416 structures. Also in case of pitched roofs, roof height seems to have a crucial impact. For street
417 canyons with pitched roofs on both sides and $AR = 1$, Xie et al. (2005) found a double vortex and
418 strongly reduced ventilation capacity for $Z_h/H = 1/2$ (where Z_h = roof height and H =building height),
419 where Abdulsheh and Kumar (2010) found a single vortex and induced ventilation capacity for Z_h
420 $/H < 1/6$. Xie et al. (2005) also illustrated the impact of the AR, whereas for $Z_h/H = 1/2$, a double
421 vortex structure was present for $AR = 1$ and a single vortex structure was found for $AR = 0.5$.

422 Similarly to the building height variation (Section 4.2.1), it is generally assumed that step-
423 up configurations are more favorable in terms of urban ventilation when compared to even or step-
424 down configurations (Kastner-Klein and Plate, 1999; Huang et al., 2007; Huang et al., 2009). A
425 wind tunnel study by Rafailidis and Schatzmann (1996) also suggests that, when the whole building
426 (including the slanted roof) is confined within the urban canopy of the surrounding buildings, a
427 slanted roof on the upstream building has the potential to increase canyon ventilation, lowering the
428 pollution levels by half compared to a flat-roof scenario. On the other hand, when the slanted roof
429 protrudes above the urban canopy, into the free-stream, upstream slanted roofs tend to reduce urban
430 ventilation, and downstream roofs improve in-canyon ventilation. The study by Rafailidis and
431 Schatzman (1996) therefore stresses the impact of the surrounding buildings on the formation of
432 different in-canyon flow patterns.

433 When comparing the studies on roof shape it becomes clear that most of these studies are
434 merely 2D simulations, outlying real-world urban configurations. Klukova et al. (2019) used a more
435 complex 3D CFD model with pitched roofs and found higher ventilation levels in non-uniform
436 canyons compared to uniform street canyons. It can also be concluded that in all 20 studies reported
437 in this overview, the street axis was always perpendicular to the main wind direction. Only the study
438 by Louka et al. (1998) used a parallel wind direction, but no conclusions related to roof shape were
439 made. Since the impact of roof shape was not investigated under different wind directions,
440 conclusions should be considered carefully.

441 Despite the difficulty to formulate guidelines for urban planning, most studies suggest that
442 trapezoidal and upward slanted roofs should be avoided. When simulating in-canyon ventilation and
443 pollution, the aforementioned studies also suggest that roof shape should not be neglected, whereas
444 most idealized simulations reduce the complexity of roof shapes by using flat roofs. They also
445 indicate that in case of new urban developments or building modifications, the impact of the roof
446 shape on in-canyon ventilation should be considered and thoroughly investigated.

447 4.2.4 Building permeability

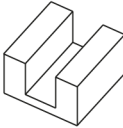
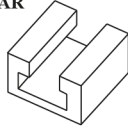
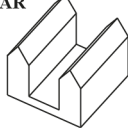
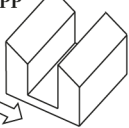
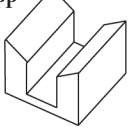
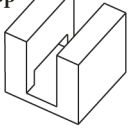
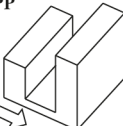

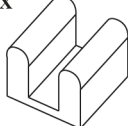
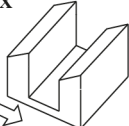
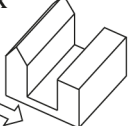
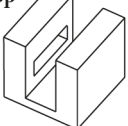
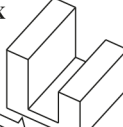
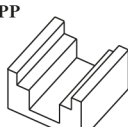
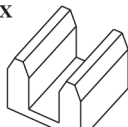

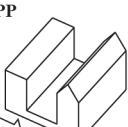
448 For the purpose of this research, building permeability is defined as the extent to which a
449 building allows wind to pass through (based on Handy et al., 2005). Permeability can be created by
450 actual voids in the building, or by open windows (defined by the window opening percentage;
451 WOP). The effect of the WOP has been thoroughly investigated by Ai and Mak (2015), Yang et al.
452 (2015, 2016), Peng et al. (2017) and Yang et al. (2020), but is less related to urban design
453 interventions and therefore not further discussed in this paper. In case of building voids, it is thought
454 that when permeability increases, a greater amount of fresh air enters the street canyon and distorts
455 the main vortex (Yang et al., 2016). In case of deep street canyons, void decks can potentially destroy
456 double vortex structures and therefore improve ventilation at pedestrian level (Zhang et al., 2017).

457 Void decks do not only result in distorted vortex structures, but also reduce the wind-pressure
458 differences across the top of the street canyon, which induces the air exchange rate between the
459 street canyon and the free surface layer. This leads to less pollutants reentering the street domain
460 and therefore pollutant dilution is improved. Both phenomena (distortion of vortex structure and
461 reduction of wind-pressure difference at the top of the street canyon) potentially result in a pollution
462 level decrease (Yang et al., 2016).

463 Numerous idealized studies have been conducted on void decks in different configurations
464 (e.g. Yuan et al., 2014; Fan et al., 2017; Zhang et al., 2019; Zhang et al., 2020). In general, it is
465 assumed that street canyons with void decks have better ventilation levels compared to street
466 canyons without void decks. Permeable elements at ground level (Wong and Ng, 2009; Ng and
467 Chau, 2011; Baghlad et al., 2018; Zhang et al., 2019) or at podium level (Fan et al., 2017) were found
468 effective in increasing in-canyon ventilation and a total decrease in pollution levels by a factor up
469 to 5 was found. More complex CFD simulations by Yuan et al. (2014) and An et al. (2019) also
470 show promising results when void decks are introduced in a more complex urban setting.

471 Despite the promising results of previous studies, numerous ‘side effects’ of building voids
472 have been detected and should carefully be taken into consideration. Fan et al. (2017) and van
473 Druenen et al. (2019) emphasize the impact of void decks on pedestrian comfort and state that when
474 a certain threshold value for permeability is reached (20% for deep street canyons and 10% for street
475 canyons with $AR < 2$), air quality improves but pedestrian comfort decreases. *The Guidelines for
476 Sustainable Building Design in Hong Kong* (Yang and Fu, 2019) suggest for example a minimum
477 building permeability of 20 % in dense urban areas. In cases like this, additional guidelines should
478 be formulated to ensure pedestrian comfort. It is also thought that void decks on floor level are less
479 favorable for pedestrian comfort compared to void decks at higher building levels (Chew and
480 Norford, 2018; Druenen et al., 2019). Void decks can also result in increased pollution levels in
481 street canyons or courtyards when stronger pollutant sources are present in adjacent street canyons,
482 especially in cases of $AR > 2$ (Fan et al., 2017; Gronemeier and Sühring, 2019). Also, single void
483 decks can improve in-canyon ventilation, but Ng et al. (2006), Chew and Norford (2018) and Wong
484 et al. (2020) suggest that void decks are most effective when they are combined as continuous airpath
485 through an entire urban fabric

486 Similar to previous parameters, orientation to the prevailing wind direction should be
487 considered. Most studies were conducted under perpendicular wind directions, since increasing
488 permeability is assumed most effective in this scenario (Zhu, 2016). Ng and Chau (2011) suggest
489 that in case of parallel winds, building voids interrupt the channeling effect of the street canyon, and
490 pollution levels tend to increase. Therefore, open space may not always favor the pollution removal
491 process. However, in order to draw firm conclusions, the impact of wind direction is still
492 inadequately investigated. An overall lack of field data is also notable in the mentioned studies.
493 Regarding urban planning, it seems legit to state that increased building permeability can be
494 beneficial for in-canyon ventilation, especially when the permeability is improved at ground level.
495 However, especially in deep street canyons, ground-level permeability can result in strongly
496 enhanced wind speed, resulting in an unfeasible pedestrian micro-climate. Therefore, the impact of
497 implementing void decks in a specific situation should be researched in advance and if necessary,
498 measures should be taken to ensure pedestrian comfort.

building configuration					
height variation	setback	roof shape			permeability
 even	AR  full length horizontal setback	AR  pitched	PP  upwind slanted	PP  outward slanted	PP  ground level void deck
PP  step-up	AR  full height vertical setback	X  vaulted	X  downwind slanted	X  step-down pitched	PP  first level void deck
X  step-down	PP  upper void setback	X  trapezoidal	X  inward slanted	PP  step-up pitched	

PP recommended in case of perpendicular winds
 X not recommended in case of perpendicular winds
 AR impact depends on the aspect ratio (AR) of the street canyon

Figure 4. Estimated most favorable building typologies based on a prevailing wind direction perpendicular to the axis of the street canyon.

499 4.3 In-canyon configuration

500 4.3.1 Semi-open settings

501 For the purpose of this research, in-canyon constructions such as eaves (louvers), awnings,
 502 overhangs (hanged walls), balconies, arcades, platforms and other elevated structures are assembled
 503 under the title ‘semi-open settings’. In general, the effect of these structures on the in-canyon airflow
 504 and pollutant dispersion has been widely investigated and it can be concluded that for most cases,
 505 semi-open structures limit the ventilation efficiency which results in increased pollutant levels. A
 506 number of CFD studies has been conducted recently on the presence of balconies in a street canyon
 507 (Hall et al., 2010; Montezari and Blocken, 2013; Murena and Mele, 2016; Llaguno-Munitxa and
 508 Bou-Zeid, 2018; Karkoulis et al., 2020) and show that in general, the depth of the balconies reduces
 509 the space available for flow recirculation. This reduces in-canyon wind speed and the air exchange
 510 between the street canyon and the free surface layer. Studies by Hall et al. (2010), Montezari and
 511 Blocken (2013) and Murena and Mele (2016) clearly show a significant modification of the flow
 512 field inside the street canyon when balconies are present, where several separate vortices and
 513 multiple areas of flow separation, recirculation and reattachment are created. This reduces mass
 514 transfer to the upper urban canopy layer. It is also thought that balconies have a greater influence on
 515 pollution levels near pedestrian height, compared to other in-canyon locations. A study by Llaguno-
 516 Munitxa and Bou-Zeid (2018) detected on overall in-canyon pollution increase by $\approx 10\%$ when
 517 balconies were placed on both sides of a street canyon ($AR = 1$). Near pedestrian level, a pollutant
 518 accumulation was detected under the first-level balconies, resulting of a pollutant increase by $\approx 80\%$
 519 %. A detailed monitoring campaign by Marini et al. (2015) confirmed these findings, whereas a
 520 higher exposure to PNCs (particle number concentrations) was detected near the sidewalks which
 521 were partly covered by balconies. However, it should be noted that most of the aforementioned
 522 studies only conducted research on balconies attached to the building’s facade as overhangs, and not
 523 on the arrangement where balconies are incorporated in the building volume (no reduction of the
 524 street canyon AR). Further research should be conducted on this matter.

525 Awnings, eaves, overhangs and platforms are also thought to limit ventilation in a street
 526 canyon. In general, these constructions alter the in-canyon flow structures (see Fig. 5) and increase
 527 pollution levels (Mohamad et al., 2015, Sato et al., 2015, Chomcheon et al., 2019; Ding et al., 2019;
 528 Pothiphan et al., 2019). CFD and wind tunnel studies by Hang et al. (2013, 2018) indicate an increase
 529 of air pollutant concentration when the width of overhangs increases. In contrast to open street
 530 canyons, it seems that the largest pollutant increase takes place when the wind direction is parallel
 531 (0-15°) to the street canyon axis (up to 630%; Hang et al., 2013, 2018; Hiyama et al., 2013). These
 532 finding are further supported by field measures by Weissert et al. (2018) and Lim et al. (2015). Other
 533 campaigns in Bangkok (Hiyama et al., 2011; Sahanavin et al., 2016) show a large pollution increase
 534 when comparing street canyons with and without platforms (up to 172% for PM₁₀) under
 535 approximately the same wind and traffic conditions. It should also be noted that in most CFD studies,
 536 the support structure of the platform is not taken into account, whereas they potentially increase in-
 537 canyon pollution (Suebyat and Pochai, 2017).

538 When the street canyon is completely covered by overhangs, an arcade is created which
 539 reduces wind speed significantly (Gerhardt and Kramer, 1990) and increases in-canyon pollution
 540 levels (Hang et al. 2013). However, Kim et al. (2010) showed that the arcade design (e.g. height,
 541 roof type, ventilation openings) has a large impact on ventilation efficiency.

542 For the purpose of urban planning, it can be concluded that all semi-open constructions
 543 have the tendency to reduce in-canyon ventilation, from small balconies to large overhangs and
 544 platforms. This would suggest that semi-open settings should be avoided in a street-canyon setting.
 545 However, in most cases, semi-open settings are constructed to protect pedestrians from specific
 546 weather conditions such as heat and heavy rain or wind, which conflicts with previous findings
 547 regarding air quality and ventilation. This illustrates the necessity to search for innovative and more
 548 flexible solutions (e.g. retractable awnings) in street canyons.

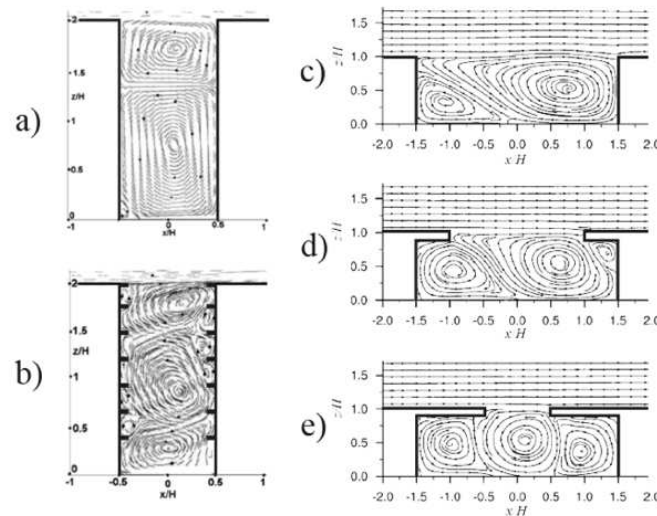


Figure 5. Estimated impact of balconies (b) and overhangs (d,e) on vortex structure in narrow (a,b) and wide (c,d,e) street canyons. With a and b retrieved from Karkoulas et al. (2020) and c, d and e modified after Mohamad et al. (2015).

549 4.3.2 Trees

550 Initially it was thought that trees improve air quality due to their capability of depositing
 551 particulate pollution (PM_{2.5} and PM₁₀) and decreasing gaseous pollutants such as NO_x and O₃
 552 (Abhijith et al., 2017). However, numerous studies concluded that an increase of pollutant
 553 concentration can possibly occur when trees are present in a street canyon configuration as a result
 554 of reduced wind speed and air exchange (Buccolieri et al., 2009; Gromke and Ruck, 2007, 2009,
 555 2011; Buccolieri et al., 2011; Salim et al., 2011; Ng and Chau, 2012; Salmond et al., 2013; Di
 556 Sabatino et al., 2015; Karttunen et al., 2020). In most wind tunnel and CFD studies, a large increase
 557 in air pollution is found near the leeward facade, and a small decrease near the windward facade
 558 when perpendicular winds occur. However, field studies (Salmond et al., 2013; Di Sabatino et al.,
 559 2015) reported no pollutant decrease at the windward facade, and thus a pollutant increase on both

560 facades of the street canyon. For parallel winds, conflicting results were found in different studies,
561 where some studies indicate increased air pollution on both sides of the street canyon and higher
562 concentration levels towards the outer end of the street canyon (Abhijith and Gokhale, 2015;
563 Buccolieri et al., 2011; Gromke and Ruck, 2012; Wania et al., 2012) and other studies indicate a
564 general decrease in air pollution levels (Amorim et al., 2013; Jeanjean et al., 2016; Buccolieri et al.,
565 2018). Oblique wind directions were reported by Gromcke and Ruck (2012) and Buccolieri et al.
566 (2015) as the worst background conditions, with the highest increase in pollution levels on the
567 leeward and windward facade. In all studies the increase/decrease of air pollutants due to the
568 presence of trees varies widely. Changes in concentration levels on the leeward facade vary for
569 example by -39 % (Xue and Li, 2017) to +164 % (Wang et al., 2018).

570 The differences in results can be explained by the high number variables which were
571 detected amongst the studies. Besides the impact of wind direction, eight essential variables were
572 found: (1) wind speed and particle size (Janhäll, 2015; Abhijith et al., 2017), (2) the amount of
573 pollution (Li et al., 2013), (3) the AR of the street canyon (Buccolieri et al., 2011; Ng and Chau
574 2012), (4) the tree planting density (Ng and Chau, 2012), (5) tree crown porosity and (6) leaf area
575 density or LAD (Salmond et al., 2013; Abhijith and Gokhale, 2015; Xue and Li, 2017; Buccolieri
576 et al., 2018), (7) trunk height and (8) stand density which refers to the actual density of the trunk
577 (Abhijith and Gokhale, 2015; Huang et al., 2019b). In general, it can be concluded that trees with a
578 high tree crown porosity, low LAD, low stand density and low trunk height are preferred in a street
579 canyon configuration (Salmond et al., 2013; Abhijith and Gokhale, 2015; Janhäll, 2015; Xue and
580 Li, 2017; Buccolieri et al., 2018; Huang et al., 2019b). In case of deep street canyons ($AR > 2$) the
581 change in ventilation performance was indicated to be less sensitive to tree planting (Buccolieri et
582 al., 2011; Ng and Chau, 2012)

583 Previous variables indicate that the effect of trees on the distribution of air pollutants in
584 street canyons is very specific for different urban environments and tree types. Therefore,
585 decisions in urban planning regarding planting/removing trees in street canyons should be
586 carefully considered and supported by detailed CFD models and field measurements.
587 Nevertheless, the decisions in relation to tree planting in street canyons should also carefully be
588 weighed against other benefits like cooling effects and energy saving (Ng and Chau, 2012).

589 *4.3.3 Hedges, low boundary walls and parked cars*

590 Similar to trees, hedges can be planted in a street canyon configuration. A number of studies
591 have been conducted on this issue (Keuken and Van Der Valk, 2010; Wania et al., 2012; Vos et al.,
592 2013; Chen et al., 2015; Gromke et al., 2016; Lazzari et al., 2016, Li et al., 2016; Ottosen and Kumar,
593 2020) suggesting that hedges can act as barriers for lateral dispersion of air pollution emitted by
594 road traffic with only limited absorption of air pollutants. Therefore, similar to trees, the
595 aerodynamic effect of hedges is shown to be much stronger than the pollutant removal capacity (Vos
596 et al., 2013). In general, most studies show lower pollution levels (24 % to 61 % lower) behind the
597 hedge (sidewalk) compared to the pollution levels in front of the hedge (roadside) (Li et al., 2016;
598 Abhijith et al., 2017). Field observations by Keuken and Van Der Valk (2010) and Ottosen and
599 Kumar (2020) confirmed these findings, with concentration reductions by 27 % to 52 % behind the
600 hedge compared to the roadside values. These results show that a hedgerow can potentially have a
601 positive effect on the air quality at pedestrian level, however on the roadside, a pollution increase
602 (up to 44%) is likely to occur (Li et al. (2016). The impact of hedgerows is also strongly affected by
603 the porosity of the hedge (Vos et al., 2013; Lazzari et al., 2016), where a pollutant increase was
604 found at pedestrian level for high-porosity hedges and a pollution decrease in case of green barriers
605 (no porosity). Therefore, hedgerows with a low porosity are recommended (Kumar et al., 2019). In
606 general, hedgerows are preferably placed as close as possible to the road, with favorable dimensions
607 of 0.9-2.0 m high and 1.5 m wide (Li et al., 2016; Kumar et al. 2019).

608 Similar to hedges and green barriers, a number of studies indicate that low boundary walls
609 (LBWs) can have a positive effect on pollution concentrations at the windward and leeward facade
610 and also result in an increased pollution near the road axis (McNabola et al., 2009; Gallagher et al.,

2015; Kristof and Papp, 2018; Baghlad et al., 2018). In most studies, two scenarios are investigated: (1) two LBWs on both sides of the road and (2) one central LBW, separating the traffic lanes. Studies by McNabola et al. (2009) and Kristof and Papp (2018) indicate that a central LBW could be most beneficial in case of winds perpendicular to the axis of the street canyon, with potential pollutant reductions up to 40 % at pedestrian height. Due to the presence of the central LBW, the vortex structure is largely altered, improving vertical dilution of air pollutants. In this scenario, a sharp pollution increase is detected near the LBW. In case of parallel winds, McNabola et al. (2009) states that two LBWs on both sides of the road are more effective, resulting in a potential pollutant decrease at pedestrian level up to 75 %. Despite these promising results, a CFD study by Wang et al. (2017b), which incorporated a dynamic wind field (changes in magnitude of the boundary layer inflow) and traffic flow, suggests that for certain wind conditions and traffic intensities LBWs could increase pedestrian exposure to air pollutants by 12-23 %. This mainly happens when wind speeds are low and the LBW weakens the wind speed even further, which results in a gradual accumulation of the in-canyon air pollutants.

Studies by Abhijith and Gokhale (2015), Gallagher et al. (2011) and Gallagher and Lago (2019) indicate that roadside parked or stationary cars can also act as a LBW. However, the effect of parked cars largely depends on the parking arrangement (parallel/perpendicular/oblique parking). Based on Gallagher et al. (2011) and Abhijith and Gokhale (2015) it can be concluded that in case of a street canyon with $AR = 1$, parallel parking seems generally preferable (potential reduction in pollutant levels by 15 % at the leeward facade and 30 % at the windward facade). However, for an oblique wind direction, every parking arrangement resulted in increased pollution levels at the windward (up to ≈ 10 %) and leeward (up to ≈ 23 %) facade. A study by Gallagher and Lago (2019) even reported a pollution increase of 32 %-62 % at the windward facade and a largely variable impact at the leeward facade ranging from -160 % to +62 %. Gallagher and Lago (2019) conclude that under low wind speed conditions, similar to LBWs, pollutant can get trapped at the windward and leeward footpath, resulting in increased pollution levels at pedestrian height.

For the purpose of urban planning it can be concluded that in general, dense hedges, LBWs and parallel parked cars can potentially shield pedestrians from high concentrations of air pollution, but only in case of high wind speeds and parallel or perpendicular wind directions. In case of low wind speeds, deep street canyons or oblique wind directions, an aversive effect could be generated. This indicates the necessity of conducting research on the average effect of these interventions, where varying wind conditions (direction and speed) should be incorporated.

4.3.4 Lane position

In most studies, a street canyon is modelled with a pollution source at the center of the road, representing pollution by traffic. As shown previously, numerous studies have been conducted on changing different variables, but few studies conducted research on the lateral displacement of the pollution source. In general, it is clear that a lateral displacement of the pollutant source does not alter the in-canyon flow structure, but it is assumed that it still can affect the dispersion process substantially (Chan et al., 2001). Studies by Kastner-Klein and Plate (1999), Chan et al. (2001), Liu and Barth (2002) and Huang et al. (2015) found a pollution reduction (by a factor up to 2) at human respiration level near the leeward wall when the traffic lane was laterally repositioned towards the windward wall. In general, the overall pollution retained by the street canyon and the pollution levels near the windward facade seem merely affected by the source position. However, when placed too close to the leeward wall, pollutants can get trapped in the small corner vortex in the lower region of the windward wall, resulting in a steep increase in pollution levels on the windward footpath (Huang et al., 2015). When traffic lanes are placed at the central axis of the street canyon, the number of traffic lanes can possibly still impact pollution dispersion. Kastner-Klein and Plate (1999), Jicha et al. (2000) and Tan et al. (2019) suggest that one central lane with traffic in one direction is more beneficial for air quality compared to two lanes, given the traffic intensity stays the same. It is thought that one central lane promotes equal distribution of pollutants at the windward and leeward side of the street canyon, which reduces pollutant peaks (Tan et al., 2019). It should be noted that

663 the aforementioned studies are all carried out under perpendicular wind direction. Therefore, the
664 effect of lane displacement is still uncertain under varying wind directions.

665 Regarding urban planning, it can be concluded that the lateral repositioning of traffic lanes
666 can potentially be a useful tool to reduce the pedestrian exposure to air pollutants. Therefore, it
667 seems interesting to reconsider the classic street layout with central car lanes and to introduce
668 asymmetric street profiles. However, the most preferable street layout depends on site-specific
669 variables and should therefore be modelled and researched in advance. In any case, side effects (such
670 as noise nuisance) and the impact on the pedestrian experience should be carefully considered.

671 *4.3.5 Additional findings*

672 During the literature review, a number of in-canyon parameters were found which were
673 less suitable for the aforementioned categorization, but which are still worth mentioning. Few
674 studies (Litschke and Kuttler, 2008; Lazzari et al., 2016; Pugh et al., 2016; Qin et al., 2018) have
675 been carried out on the impact of green walls on air quality in a street canyon configuration. These
676 studies estimate a reduction in concentration levels by 9 % - 34 % (CO₂), 23 % - 29,3 % (PM₁₀) and
677 15 % (NO₂) due to the presence of green walls, however due the lack of further research, these
678 results should not be generalized. Litschke and Kuttler (2008) estimated that extensive greening
679 (with trees and maximal facade greening) could be within the bounds of possibility to compensate
680 for local vehicle emissions. However, the study takes into account a 100% facade greening, which
681 is in most cases impossible due to window openings and other irregularities. Also, the negative effect
682 of vegetation on the in-canyon ventilation capacity has not been taken into consideration.
683 Notwithstanding the uncertainties, studies of Vos et al. (2013) and Kumar et al. (2019) advise to use
684 green walls in most canyon configurations. The research conducted on the effect of green roofs in
685 street canyons is also fairly limited, but a rather minor impact can be expected (Pugh et al., 2012;
686 Baik et al., 2012; Speak et al., 2012; Qin et al., 2018).

687 It was also found that in field studies, in-canyon flows are largely altered by small-scale
688 elements (Karra et al., 2017). Gavey and Savory (1999) described these obstacles (e.g. small
689 constructions, kiosks and stationary vehicles) as in-canyon roughness elements which create
690 complex in-canyon flow patterns. A CFD study by Lin et al. (2019) for example indicates that all
691 types and arrangements of wall-hanged advertisement boards result in increased in-canyon pollution
692 levels. On a very small scale, Jiang et al. (2019) discovered that even wall elements such as louver
693 blinds could reduce in-canyon ventilation, since sub-vortices are generated between the louver
694 blinds, decreasing the wind speed near the facade.

695 Previous findings indicate that small-scale roughness elements can large affect local
696 pollution concentration. The results however depend on site-specific conditions and meteorological
697 variables. Therefore, the usage or destruction of roughness elements in urban planning should be
698 careful considered and analyzed on the level of one specific site.

699 **5. Guidelines**

700 *5.1 Guidelines for urban planning and implementation strategy*

701 It is clear that, despite the high number of reviewed studies, no rigid guidelines to enhance air
702 ventilation can be formulated due to the high number of variables that should be considered.
703 However, this study aims to formulate a number of guidelines that can be used as a rule of thumb
704 for urban planners. In urban planning, it is clear that different cities have different planning systems
705 and thus different stages in which these guidelines can be implemented. However, in general, some
706 similarities between most planning systems can be found, such as the existence of hierarchic
707 planning levels (state/province/city/county/districts) and a presence of a spatial policy framework to
708 guide spatial interventions (Jain and Pallagst, 2015; Biesewig, 2016; Meng et al., 2020). On city
709 level, overall city plans (or city master plans) and city regulatory plans are mostly supported by
710 specialized subject plans (SSP) which all together represent the overarching spatial framework for

711 construction projects (Meng et al., 2019). Based on the implementation strategy of the air ventilation
 712 assessment (AVA) of Hong Kong (Ng, 2009), a distinction has been made between guidelines
 713 applicable on city-wide scale and guidelines applicable on a local project scale. On the city-wide
 714 scale, quantitative guidelines can be formulated in a SSP (e.g. ventilation plan) which can be used
 715 to assess project proposals/areas against pre-set design parameters and criteria (e.g. permeability or
 716 BHR).

717 On the other hand, numerous guidelines can be derived which are not suitable for translation
 718 into quantitative guidelines. Ng (2009) suggests therefore the development of a number of
 719 qualitative guidelines which provide designers with a strategic sense on how to improve the
 720 ventilation capacity in their projects. All aforementioned guidelines are brought together in Table 2,
 721 and an indication has been made on their applicability for specialized subject plans (SSP) or for
 722 qualitative guidelines for urban planners (QG). It should be noted that some of these guidelines are
 723 in need of further research before implementation.

Table 2. Guidelines for the optimization of the ventilation capacity in street canyons, with a selection of quantitative guidelines suitable for a specialized subject plan (SSP) and qualitative guidelines (QG)

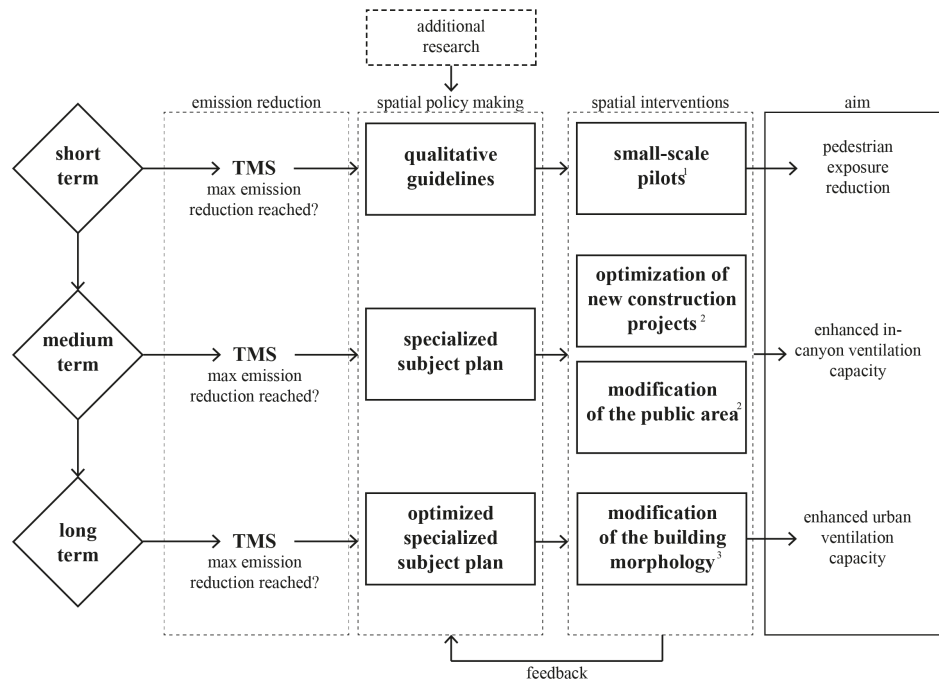
Configuration level	Guidelines	SSP	QG
Street-canyon config			
- Orientation	- A parallel orientation of the street canyons axis towards the main wind direction seems preferable to improve in-canyon ventilation. When oriented oblique or perpendicular to the main wind direction (and AR > 0.65), additional measures have to be taken to ensure a sufficient ventilation capacity.	x	
- Aspect ratio (AR)	- Lower ARs are recommended to improve in-canyon ventilation. Street canyons with AR < 0.65 tend to be less vulnerable for pollutant accumulation. Once AR > 0.65, additional measures have to be taken to ensure a sufficient ventilation capacity.	x	
- Street canyon depth	- In deep street canyon, the threshold value of AR = 5.0 should be respected in order to avoid limited ventilation and peak pollution levels at pedestrian height. - Wind catchers may improve in-canyon ventilation in deep street canyons.	x	x
- Street canyon length	- Limiting the street canyon length improves in-canyon ventilation and therefore enhance pollution dispersion and dilution. In general, the lateral aspect ratio should not exceed the threshold value of LAR = 3.0.	x	
Building configuration			
- Building height variation	- Increasing the building height variation results in increased turbulence, which potentially improves pollutant dilution and in-canyon ventilation. Homogeneous building heights should be avoided if possible. - A step-up configuration towards the main wind direction is preferable to improve ventilation.	x	x
- Building setback	- Building setbacks seem potentially favorable to reduce in-canyon pollution levels, whereas in case of perpendicular winds, full-length horizontal setbacks seem more favorable in deep street canyons (AR > 2) and full-height vertical setbacks are recommended in regular street canyons (AR < 2).		x
- Roof shape	- In street canyons with a low AR < 1, pitched roofs can improve ventilation. Once AR > 1, all roof typologies seem to limit in-canyon ventilation compared to a flat-roof situation. - Inward-slanted, upward slanted and trapezoidal roofs seem less favorable in terms of in-canyon ventilation and should therefore be avoided if possible.		x
- Building permeability	- Ground-level permeability seems highly effective in dispersing pollution and reducing pollution levels near pedestrian height. A building permeability of 20 % is recommended in dense urban areas.	x	
In-canyon configuration			
- Semi-open settings	- All semi-open settings tend to reduce ventilation and should therefore be limited or replaced by flexible solutions.	x	
	- Hanged balconies should be avoided. When balconies are applied, they should be placed in the building volume in order to avoid a reduction of the AR and thus the ventilation capacity.	x	
- Trees	- Tree species with a lower crown and stand density are recommended in order to allow wind penetration. Trunk heights are preferably low.	x	
- Hedges and low boundary walls	- Hedges should be placed close to the pollutant source and should be less permeable by wind, in order to serve as a barrier which reduces pedestrian exposure to air pollution. - Under perpendicular wind conditions, LBWs may reduce pedestrian exposure to air pollution. A central LBW seems more effective than 2 roadside LBWs.		x
- Source position	- Under perpendicular wind conditions, a lateral displacement of the source towards the windward facade reduces pedestrian exposure to air pollution.		x
- Additional findings	- Green walls seem to have a very modest impact on the ventilation capacity but may enhance the deposition of PM and are therefore generally recommended.	x	
			x

724 It is clear that most guidelines suitable for SSP are generally well investigated, whereas for
725 most qualitative guidelines, the results are largely dependent on site-specific characteristics.
726 Therefore, it is suggested these guidelines are always subjected to a preliminary (CFD) study and a
727 multiple scenario's which alter these parameters in a specific street canyon under different
728 meteorological condition are tested. Since it is proposed to integrate these guidelines in urban
729 planning, it is important to bare in mind other parameters such as for example the pedestrian comfort
730 or ecological value/cooling effect of trees. High wind speeds may favor pollution dispersion and
731 dilution but can also create uncomfortable environments for pedestrians (Lenzholzer, 2015). The
732 study by Fan et al. (2017) on building permeability already takes pedestrian comfort related to wind
733 speed into account. However, in most other studies, this point of view is fairly neglected. It is self-
734 evident that for the purpose of urban planning, the positive effect of increased wind speed on
735 reducing pollution levels should be carefully weighed against the potential loss of pedestrian comfort
736 and emotional wellbeing.

737 It is also clear that the spatial implementation of these guidelines is largely time-dependent. In
738 case of an existing urban fabric, the morphology of the street canyon configuration and building
739 configuration is rather static compared to the in-canyon configuration. Implementing guidelines on
740 the street canyon and building configuration is less evident and demands a long period of
741 implementation time which contradicts to the urgent demand to improve air quality in street canyons.
742 Therefore, a time-dependent implementation strategy is suggested, represented in Fig. 6. For every
743 time period (short, medium and long term) it is suggested that firstly the traffic management
744 strategies (TMS) are reviewed and optimized in order to maximize pollutant reduction. On the level
745 of spatial policy making, a number of qualitative guidelines can already be drafted based on the
746 preliminary research in a short-term period (< 1 year). These guidelines can be used to produce a
747 number of "small-scale pilots" such as the implementation of LBWs or the removal of in-canyon
748 wind obstacles (e.g. billboards) which aim to contribute to the short-term goal of decreasing the
749 pedestrian exposure to air pollution. Before implementing these interventions on a city-wide scale,
750 the pilots should be tested and used for further validation of the implemented measures. On a
751 medium-term time frame (1-3 years), the SSP (e.g. ventilation plan) can be developed as a spatial
752 policy framework to guide the optimization of new construction projects and the modification of the
753 public area. The main aim of the framework should be to enhance/improve the in-canyon ventilation
754 capacity.

755 By conducting additional research and investigating the implemented guidelines on-site, an
756 optimization of the qualitative guidelines and the SSP can be developed on the long-term period.
757 Within this long-term time frame, the ambition should be to be able to apply justified modifications
758 to the existing building morphology (e.g. varying building height or increasing building
759 permeability), with the ambition to improve the urban ventilation capacity. However, these measures
760 demand longer implementation terms (up to 10 years). The impact of all spatial interventions should
761 be investigated in time, in order to generate feedback to optimize the policy making process. By
762 doing this, an iterative optimization process is developed.

763 For most urban planners, the first and second part of the strategy is generally interesting,
764 since the ability is created to improve air quality by small and short-term modification in the public
765 terrain. For city planning in general, the threefold part of this strategy indicates the necessity to
766 develop short-term, mid-term and long-term strategies to assess air quality and ventilation in street
767 canyons. Still, it is highly important to emphasize that designing for improved ventilation in street
768 canyons is a highly complex matter, and a high number of limitations and variabilities should be
769 kept in mind. This indicates that none of the aforementioned guidelines should be implemented on
770 site without additional research or validation by (CFD) models.



1. limited amount of general guidelines, detailed CFD study necessary
2. some general guidelines are applicable but a high number of variabilities should be taken into account, detailed CFD study necessary
3. general guideline are applicable in most cases, CFD study recommended for specific cases

Figure 6. Potential implementation strategy of the guidelines to improve air quality in street canyons based on the implementation time (Source: author)

771 5.2 Limitations and variabilities

772 For complex building arrangements (real cities) with buildings varying in height and shape
 773 and different spacing between buildings, the flow field will most likely be a complex combination
 774 of 3D vortices and channelized flow (Brown, 2004). Figure 7 illustrates that these complex flow
 775 fields even exist for idealized street canyons, with more complex vortices than shown in previous
 776 visualisations. Kim and Baik (2004) illustrate the emerging of complex portal and roll-type vortices
 777 for an idealized street canyon (W/H -ratio = 1) with perpendicular wind. The study also indicates
 778 that slight changes in wind direction ($5^\circ \leq \theta \leq 20^\circ$) can distort the shape of the vortices (see Fig 7a,b).
 779 Another study by Yang and Fu (2019) indicates the presence of very complex wind patterns in
 780 existing urban environments (Fig 7e). Therefore, it should be noted that the representations in
 781 previous sections are simplified, and more complex flow fields are likely to appear.

782 Brown (2014) and Wood et al. (2009) also indicate the complexity of flow fields near the
 783 end of a street canyon or near intersections. Sudden changes in building heights (such as high-rise
 784 buildings) are also thought to have a large impact on the local air flow fields. This observation
 785 already illustrates the impact of variabilities and uncertainties, which is an inherent characteristic of
 786 the real-world wind field (Neophytou et al., 2011). This variability is created by urban morphology,
 787 ambient and meteorological conditions (e.g., wind speed and wind direction), atmospheric stability,
 788 source strength of pollutants and the effect of solar irradiation (Kim and Baik, 1999, Yazid et al.,
 789 2014). In numerous CFD studies, the impact of the surrounding built-up area is neglected or reduced
 790 to a very simplistic representation. A study by Michioka and Sato (2012) suggests that, even when
 791 idealized, the shape of the surrounding environment influences the turbulent structure of the
 792 incoming wind near the street canyon, and therefore affects the pollution dispersion process.
 793 Therefore, it can be concluded that a more complex modeling of the direct urban environments of a
 794 street canyon (e.g., Moon et al., 2014) could be beneficial for obtaining more realistic results. Not
 795 only the urban form, but also the presence of other pollutant sources in the environment could affect
 796 in-canyon pollution levels. On a large scale, transboundary pollutants can affect in-canyon pollutant
 797 levels. Other pollutant sources could be traffic in adjacent street canyons (Dabberdt and Hoydysh,
 798 1991) or even pollution (especially PM) from chimneys on adjacent roofs (Badas et al., 2018). On

799 a local scale, moving vehicles, trees, and exhaust vents among other things initiate further
800 complications (DePaul and Sheih, 1985; Brown, 2004; Yazid et al., 2014). It should be emphasized
801 that the impact of these pollutants can largely affect the dispersion procedures.

802 Numerous studies on wall heating (Sini et al., 1996; Kim and Baik, 2001; Xie et al., 2005;
803 Offerle et al., 2007; Kang et al., 2008; Park et al., 2012; Nazarian and Kleissl, 2016; Allegrini, 2018;
804 Hang et al., 2019) indicate that uniform and nonuniform wall heating (solar-induced or due to
805 anthropogenic heating of the building interiors) or ground heating strongly affects the in-canyon
806 vortex formation due to the development of buoyancy driven flows near the surface. In most cases,
807 wall or ground heating will improve in-canyon ventilation and therefore reduce pollution levels
808 (Kim and Baik, 2001; Kang et al., 2008; Nazarian and Kleissl, 2016). However, Xie et al. (2005)
809 indicate that this effect largely depends on which surface (leeward/windward facade or ground) is
810 heated. The effects of wall heating should carefully be considered, since this indicates that in-canyon
811 flow patterns can change during long-term seasonal transitions or even short-term solar changes
812 (Offerle et al., 2017). However, the aforementioned field study by Offerle et al. (2017) also indicates
813 that buoyancy effects from the heated walls seem to have less impact on in-canyon flow regimes in
814 real situations (field measurements) compared to the estimated impact shown in numerical
815 experiments.

816 Lastly, it should be stressed that most of the guidelines are derived from studies which use
817 passive scalars (e.g. CO / CO₂) or only introduce one traffic-related pollutant (a summary of all
818 pollutants per reviewed study can be found in the **Appendix**). Therefore, these guidelines are
819 applicable for most of these pollutants (PM, NO_x / NO₂, CO / CO₂). However, it should be stressed
820 that results can vary due to the different behavior of pollutants, especially due to deposition effects
821 when for example green infrastructures are introduced (e.g. Vos et al., 2013; Buccolieri et al., 2018).
822 Furthermore, traffic-related emissions consist mostly of reactive pollutants, such as nitrogen oxides
823 (NO_x=NO+NO₂), volatile organic compounds (VOCs) and secondary pollutants (e.g. ozone, O₃).
824 The chemical reaction between these reactive pollutants can alter the dispersion process (Zhang et
825 al., 2020). CFD studies (Kwak and Baik, 2012; Park et al., 2015) and field measurements (Kwak et
826 al., 2016) on multiple reactive pollutants (NO, NO_x, VOCs and O₃) found a reduction in NO₂ and
827 O₃ levels when NO levels increased due to the NO_x-O₃ photochemistry. Therefore, street canyons
828 with higher NO_x values tend to have lower O₃ concentrations than the background concentration.
829 This indicates that, due to chemical reactions, the aforementioned guidelines are less suitable for
830 reducing O₃ values, and their impact on other reactive pollutants should be reconsidered based on
831 the potential chemical reactions.

832 Despite these issues, Neophytou et al. (2011) conclude that computational models such as
833 CFD models are suitable for predicting flow fields and dispersion patterns, but the given variability
834 and uncertainty in the field should always be considered.

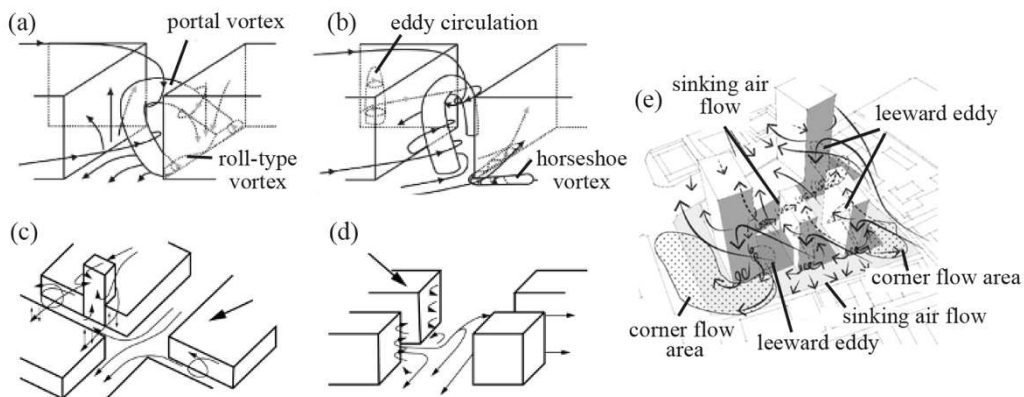


Figure 7. Complex flow fields for different urban morphologies with: (a) a schematic representation of complex 3D vortices in an idealized street canyon with perpendicular wind and (b) oblique winds (Kim and Baik, 2014), (c,d) assumed flow fields in complex urban environments (near intersections and high-rise buildings, based on Wood et al., 2009) and (e) assumed flow patterns in a real urban environment (Yang and Fu, 2019)

835 *5.3 Advantages and limitations of CFD modelling*

836 Previous findings indicate the necessity to validate urban design interventions and their
837 impact on local air quality in street canyons. In the reviewed studies, CFD is used as a validation
838 tool (see **Appendix**). In most cases, CFD modelling is a cost-effective way for evaluating the effects
839 of air pollution mitigation strategies (only in case of Reynolds-averaged Navier Stokes (RANS)
840 studies, Large Eddy Simulations (LES) are, however, much more time consuming and costly).
841 Urban CFD simulations, however, require specific care in order to obtain reliable results. CFD
842 simulations should therefore be performed in accordance with existing best practice guidelines (e.g.
843 Franke et al., 2007; Blocken et al., 2007; Tominaga et al., 2008). Elaborate reviews dealing
844 specifically with this matter are also available in the literature (e.g. Blocken et al., 2011; Lateb et
845 al., 2016; Blocken et al., 2014; Moonen et al, 2012). CFD studies should, moreover, be validated
846 with experimental data (Moonen et al, 2012) from field measurements or databases with
847 experimental data (e.g. CODASC, n.d.; CEDVAL, n.d.; CEDVAL-LES, n.d.; AIJ, n.d.; Joint Urban
848 2003, 2003).

849 In addition to the care that urban CFD studies require, important problems in this research
850 field have yet to be resolved, since inaccurate results and deviations from reality are still obtained
851 in CFD models (Blocken et al., 2016; García-Sánchez et al., 2018). In general, it is concluded that
852 most computational models are suitable to predict time-averaged concentrations, but maximum
853 concentrations vary greatly and are therefore difficult to predict. Despite the current problems in
854 urban CFD modelling, it is expected that it will increasingly be used for evaluating urban air
855 pollution, since it is a very active field and its strategies and methodologies are still evolving. In
856 general, as displayed by many studies mentioned in this literature review, CFD has become a
857 powerful tool for modeling the impact of urban design interventions on the ventilation performance
858 and air quality in street canyons. However, due to the complexity and unresolved issues of CFD, it
859 is not a feasible tool to be used by urban planners. This indicates the necessity for a closer
860 collaboration between engineering sciences and urban planning.

861 **6. Conclusion**

862 For the purpose of urban planning, a broad literature review was conducted on 12 spatial
863 parameters which potentially affect the in-canyon ventilation capacity of urban street canyons. The
864 aim of this literature review was to formulate a number of spatial guidelines for urban planners, as
865 a supplement to the traffic management strategies that are applied in several cities. More than 200
866 fragmented studies were reviewed and brought together in a comprehensive overview. Hereby, a
867 thorough overview is created and 18 general guidelines were derived from the reviewed studies. An
868 implementation strategy of this guidelines is suggested, where some guidelines are more likely to
869 support the policy framework and other more qualitative guidelines can be used to guide urban
870 planners. However, by doing the literature review, a large number of uncertainties, variabilities and
871 limitations were detected, which should be born in mind by urban planners. The literature review
872 also indicated CFD-modelling as a useful tool to validate the implementation of different design
873 measures. However, for the usage of CFD, a closer collaboration between engineering sciences and
874 urban planning is recommended.

875 An additional value of this literature review is the detection of knowledge gaps. It is clear
876 that some parameters (e.g. building setback) are still in need of further investigation. Also, few
877 studies were conducted using variable wind conditions (e.g. wind direction and speed), which
878 reduces the reliability of the results when compared to realistic situations. This indicates the
879 necessity of studies which use a realistic probability distribution for the wind conditions, in order to
880 develop more realistic insights on the average impact of different measures. It is also clear that only
881 few studies (e.g. Abhijith and Gokhale, 2015; Hao et al., 2019) were conducted on combining
882 multiple of the aforementioned parameters (e.g. building height variation, roof shape, source
883 position), hence the potential synergies between these parameters can still be explored. Lastly, the

884 number of field studies seems scarce compared to wind/water tunnel or CFD studies (in only 28
885 studies field measurements were used, in contrast to 137 studies which used CFD or a wind/water
886 tunnel setup, see **Appendix**). This indicates the necessity of more field studies, to test and
887 complement the mere computational studies.

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