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# Accelerated Methane Storage in Clathrate Hydrates Using Mesoporous (Organo-) Silica Materials

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#### ABSTRACT

Methane (CH<sub>4</sub>) clathrate hydrates have gained much attention in the ever-growing search for novel energy storage methods; however, they are currently limited due to their poor water-tohydrate conversions and slow formation kinetics. To surmount these bottlenecks, significant research has been centered on the design of novel methods (porous media). In this vein, the present work explores two hydrophobic mesoporous solids, an alkyl-grafted mesoporous silica (SBA-15 C8) and a periodic mesoporous organosilica (Ring-PMO), in their ability to promote CH<sub>4</sub> clathrates. Both materials have shown to facilitate CH<sub>4</sub> clathrate formation at mild operating conditions (6 MPa and 269 K to 276 K). The study revealed that the maximal CH<sub>4</sub> storage capacities are strongly linked to the critical/optimal quantity of water in the system which was determined to be at 130% and 200% of the pore volume for SBA-15 C8 and Ring-PMO, respectively. Up to 90% and 95% of the maximum water-to-hydrate conversions were achieved in 90 min at the lowest experimental temperature and critical water content for SBA-15 C8 and Ring-PMO, respectively. At these conditions, SBA-15 C8 and Ring-PMO showed a maximum gas uptake of 98.2 and 101.2 mmol CH<sub>4</sub>/mol H<sub>2</sub>O, respectively. Both the materials exhibited no chemical or morphological changes post-clathrate formations (characterized using FT-IR, N<sub>2</sub> sorption, XRD, and TEM), inferring their viability as clathrate promoters for multiple cycles. An integrated multistep model was considered adequate for representing the hydrate crystallization kinetics and fits well with the experimental kinetic data with a low average absolute deviation in water-to-hydrate conversions among the three distinct kinetic models analyzed. Overall, the results from this study demonstrate hydrophobic porous materials as effective promoters of CH<sub>4</sub> clathrates, which could make clathrate-based CH<sub>4</sub> storage and transport technology industrially viable.

KEYWORDS: Methane; clathrate; mesoporous (organo-) silica; kinetics

#### 1 1. Introduction

2 The world's energy demand is skyrocketing to bolster the expanding population and the 3 burgeoning economy. Contemporaneously, energy policies and regulations are constantly 4 evolving to emphasize using natural gas and hydrogen (H<sub>2</sub>) as crucial requirements for 5 maintaining the environment's security globally[1, 2]. Using natural gas, which has a methane 6 (CH<sub>4</sub>) content of over 95% and burns relatively clean compared to coal, could be a viable 7 transition option for meeting the energy demands right now towards a fully sustainable 8 energetic strategy[3]. Consequently, improved technologies for high-density storage and 9 transportation are key to using natural gas to its full potential. The current method for storing 10 gas in a compressed gas phase raises safety concerns due to its high-pressure requirement and 11 the flammable nature of CH<sub>4</sub>, additionally, liquifying gas for transportation is an energy-12 intensive operation, making transportation inefficient[4]. Aside from these commercially 13 available technologies, research on low-cost synthetic porous materials with high chemical, 14 mechanical, and thermal stabilities is actively being developed in pursuit of CH<sub>4</sub> storage via 15 adsorption[5-10]. Alternatively, the usage of gas hydrates is a novel and intriguing alternative 16 technology that has received significant attention for high-density CH<sub>4</sub> storage and 17 transportation[11-13].

18 Gas hydrates or clathrates are crystalline compounds that potentially form at high pressures 19 and low temperatures when non-polar gases are trapped within solid water (H<sub>2</sub>O) lattice 20 (polyhedral cavities), where a unit volume of hydrate can deliver approximately ca. 160  $m^3$  of 21 CH<sub>4</sub> at standard conditions[14]. This substantial increase in energy density can highlight that 22 CH<sub>4</sub> hydrate or clathrate could be an economically advantageous alternative storage 23 technology. However, the commercialization of hydrate technology is stymied by several 24 challenges and is not yet industrially competitive with conventional storage and transport 25 technologies owing to its poor water-to-hydrate conversions and slow kinetics caused by

26 inadequate mass transfer between hydrate forming gas/H2O and inefficient removal of 27 hydration heat that does not promote hydrate growth[15, 16]. Enhancement of mass and 28 hydration heat transfer has been the subject of extensive research using various approaches 29 such as reactor design (stirred tanks[17-22], spray nozzles[23-26], bubble columns([27, 28]), kinetic/thermodynamic promoters (sodium dodecyl sulfate (SDS)[29-31], SC<sub>12</sub>S[32], and 30 31 tetrahydrofuran (THF)[33-35]). However, these approaches also possess certain limitations 32 that preclude achieving high-density storage[36]. A comprehensive review and list of 33 kinetic/thermodynamic promoters for CH<sub>4</sub> hydrates are presented by Nasir et al.[37] and 34 Kummamuru et al.[36], respectively.

Besides reactor designs and promoters, continuous research efforts[38-40] have 35 36 demonstrated that synthetic porous materials (in fixed-bed columns) can accelerate the kinetics 37 of hydrate formation and water-to-hydrate conversion and the current research is progressing 38 in investigating such potential porous materials with some of the actively pursued materials 39 being silica-based materials [41-60], carbon-based materials[61-76], metal-organic 40 frameworks[77-84], zeolites[85-88], glass beads[60, 89-92], interstitial space between stainless 41 steel beads/fiber[93-95], aluminum foam[96, 97] and silicon carbide[98]. Multiple variables, 42 particularly, pore confinement, gas saturation at the interface, and surface wettability, all of 43 which are influenced by surface chemistry, pore size, and geometry, play an important role in 44 CH<sub>4</sub> hydrate formation and kinetics. Recent studies have shown that hydrophobic materials are more efficient than hydrophilic materials at enhancing hydrate nucleation and growth[44, 61, 45 83, 92, 99-104]. Although hydrophobic pores seldom adsorb H<sub>2</sub>O, sudden adsorption of H<sub>2</sub>O 46 was seen in these nanopores above  $P/P^0$  (relative pressure) of 0.5, depending on surface 47 48 functional groups and pore diameters [62, 105-107]. It was also reported that H<sub>2</sub>O can be 49 adsorbed and stabilized in hydrophobic pores free from surface functional groups by cluster formation[108-110]. In addition, thermodynamic studies show that H<sub>2</sub>O molecules prefer to 50

51 minimize their free energy by clustering as they encounter difficulties in forming hydrogen 52 bonds with hydrophobic surfaces [50, 61, 111, 112]. From these investigations, it can also be 53 deduced that, unlike H<sub>2</sub>O bonding with hydrophilic surfaces, the hydrophobic materials tend 54 to have poor H<sub>2</sub>O bonding with their surfaces, which enhances H<sub>2</sub>O mobility and can promote 55 hydrate nucleation. Molecular simulations by Nguyen et al.[113] also showed enhanced local 56 gas density at the hydrophobic surface and the clustering mechanism of H<sub>2</sub>O facilitating 57 hydrate formation. Analogous research by Iiyama et al.[114] and Li et al.[115] using XRD and 58 Raman spectroscopy also corroborated these findings. Studies from Casco et al.[62] have 59 shown that hydrophobic properties of activated carbon can boost CH<sub>4</sub> hydrate growth and 60 similar research by Wang et al.[50] showed that the induction time in hydrophobic sands was 61 at least 8 times shorter than in hydrophilic sands for CH<sub>4</sub> hydrate formation. Hydrophobisized 62 fumed silica nanoparticles, on the other hand, demonstrated good promoting effects on CH4 63 hydrate formation[48, 49]. Mileo et al.[116] in their recent molecular simulation study also 64 explored the stability of CH<sub>4</sub> hydrates in different hydrophobic linkers grafted to silica-based 65 materials and concluded that a certain degree of hydrophobic linkers coupled with larger pore 66 sizes are beneficial for stabilizing the clathrate phase at 6 MPa and 260 K.

67 Considering the potential of hydrophobicity in promoting gas hydrate formation, it is 68 imperative to develop/design and investigate such a porous material to attain a maximum CH4 69 storage capacity for large-scale industrial applications. In contrast to the conventional low-70 dimensional pore sizes and networks in activated carbons, this study focuses on well-defined 71 pore structures of alkyl-grafted mesoporous silica and periodic mesoporous organosilica 72 having pore diameters approximately 6 times greater than the sI unit cell (1.2 nm) of CH<sub>4</sub> 73 hydrate[14]. Due to the sheer influence of hydrophobic pores on H<sub>2</sub>O activity, this relatively 74 large confined space can offer an interfacial area for CH<sub>4</sub> hydrate formation and also contributes 75 to promoting hydrate growth. Although both materials share similar chemical characteristics,

76 they fundamentally differ in the architecture of their pore shape, network, and size. 77 Concurrently, limited research is available in the literature [76, 117, 118] exploring the effects 78 of pore size and network on CH<sub>4</sub> hydrate nucleation and water-to-hydrate conversion. In light 79 of this, the current study aims to enhance the understanding of how the mesoporous structures of alkyl-grafted mesoporous silica, hereafter referred to as (SBA-15 C8) and periodic 80 81 mesoporous organosilica, hereafter referred to as (Ring-PMO), affect CH<sub>4</sub> hydrate 82 nucleation/formation/growth at 269 K, 274 K, 276 K and an initial pressure of 6 MPa with 83 multiple pore volume-H<sub>2</sub>O saturations. As a result, the kinetics of CH<sub>4</sub> hydrate formation, as 84 well as the effects of H<sub>2</sub>O content on gas uptake, and water-to-hydrate conversions are also investigated. 85

86

87 2. Experimental methods

88 2.1. Materials

The chemicals used in this work are listed in Table 1 and were used without any additionalpurification.

91

92 2.2. Synthesis and characterization methods

Mesoporous silica, SBA-15, was synthesized according to a classical procedure, already reported in the literature[119]. The surfactant templated synthesis involved the use of P123 as a structure-directing agent. In the first step, 4.07 g P-123 (0.7 mmol) was dissolved in a 1.68 M HCl solution containing 144.13 ml H<sub>2</sub>O (8 mmol) and 20.17 ml HCl(aq, 37%) (242 mmol), after which 9.12 ml the Si-source (41.2 mmol), in the form of namely tetraethyl orthosilicate (TEOS), was added and the whole mixture was stirred for 7.5 h at 318 K. Next, the white precipitate was aged overnight at 353 K, under static conditions. Subsequently, the white precipitate was filtered and washed with distilled H<sub>2</sub>O, dried (333.2 K), and calcined at 823 K
for 6 h (1 K/min.), resulting in the pristine SBA-15 material.

In order to alter the hydrophilic-hydrophobic properties of the SBA-15, a post-synthesis approach was employed. In the first step, 5 g of SBA-15 were dried for 3 h at 473 K and mixed with 150 mL of toluene under an inert atmosphere. After 30 min of stirring, 20 g of trimethoxy(octyl)silane was added and the mixture was stirred for 3 days at 353 K. To remove the unreacted modifier, the precipitate was filtrated and washed 6 times with 70 mL of toluene. Finally, the white powder was dried overnight at 323 K and this product is denoted as SBA-15 C8 in what follows.

109 In a general Ring-PMO synthesis, a flask was charged with a 0.96 M HCl solution, containing 110 180 ml H<sub>2</sub>O and 14.4 ml (173 mmol) HCl(aq, 37%), to which 35.04 g (470 mmol) KCl and 1.5 111 g (0.26 mmol) P-123 were added. The mixture was left to stir at 318 K until a homogeneous 112 solution with a blue hue was observed. Next, 8.16 ml (20.26 mmol) of HETSCH is added and the whole is continued to stir for 3 h at 318 K. Afterwards, the flask is put in an oven for 24 h 113 114 at 368 K to complete the organosilica network condensation after which the as-formed white 115 solid is collected through vacuum-assisted filtration. Unreacted silanes and surfactants are 116 removed through extensive Soxhlet extraction using acetone. Residually bound solvent molecules are removed from the porous solids through an activation step where the materials 117 118 are subjected to reduced pressures ( $\leq$  5E-4 MPa) at temperatures of 393 K. The yield of the 119 Ring-PMO synthesis was found to be virtually quantitative. A chemical representation of Ring-120 PMO and SBA-15 C8 is presented in Figure 1.

121 Two-dimensional transmission electron microscopy (2D TEM) pictures were taken using a 122 JEOL JEM-1010 TEM instrument operated at 100kV without spherical aberration (Cs) 123 correction. The powder X-ray diffraction (PXRD) pattern was measured with a Bruker D8 124 Advance with autochanger using Cu K-alpha irradiation with a wavelength ( $\lambda$ ) of 0.154 nm in 125 a Bragg-Brentano geometry. PXRD diffractograms were determined in the range of 0.2-10° 126 with a step-size of 0.015°. The porosity of the materials was assessed through N<sub>2</sub>-sorption, as 127 performed on a Quantachrome Quadrasorb automated sorption system operated at 77 K. Prior 128 to the analyses, the samples were degassed at 393 K for 16 h. A Nicolet 6700 Fourier Transform IR (FT-IR) spectrometer was used to perform in-situ diffuse reflectance infrared FT (DRIFT) 129 130 measurements. The samples were heated to 393 K, under vacuum, for 20 min and this 131 temperature was maintained during the spectra acquisitions. The samples were diluted in KBr (2 wt.%), and 100 scans were accumulated for each spectrum with a resolution of 4 cm<sup>-1</sup> in the 132 region of 4000–500 cm<sup>-1</sup>. Quantification of the C8 density of the SBA-15 C8 material was 133 performed through TGA analysis using a Mettler Toledo TGA/DSC 3+ star system. The 134 135 obtained TGA results were corroborated with the N<sub>2</sub>-sorption analysis (BET surface area), to 136 approximate the surface functional group density of the C8 molecule. For this, the mass loss 137 considered in the TGA-profile analysis was between 473 K and 1073 K, assuming that the 138 toluene, which was used as a solvent and washing agent during the post-synthesis modification 139 protocol, evaporates below this temperature.

140

141 2.3. Experimental apparatus and procedure

As seen from the schematic layout (Figure 2), CH<sub>4</sub> hydrate formation tests were conducted in stainless steel cylindrical reactor (effective volume: 150 cm<sup>3</sup>) purchased from Swagelok (316L-50DF4-150) which can withstand gas pressures up to 34.4 MPa. The reactor was immersed in a high-precision circulating bath (CORIO CP-1000F, JULABO GmbH) filled with a water-ethylene glycol mixture to maintain the cold and stable temperature inside the reactor. The temperature stability of the bath was  $\pm$  0.03 K. The pressure in the reactor was measured for every 1 Hz, using a pressure transmitter (PAA3X-30 MPa; KELLER AG für 149 Druckmesstechnik; a range of 0-30 MPa absolute, with  $\pm$  0.01% FS accuracy). The methane 150 gas (99.99% purity) used in this study was supplied by Air Liquide Benelux Industries.

151 A standard method was employed to investigate the CH<sub>4</sub> hydrate formation and the 152 experimental procedure is described as follows. Prior to the commencement of experiments, 153 the reactor was cleaned with H<sub>2</sub>O and dried, followed by adding 1 g of synthesized material 154 (dried at 343 K overnight) and a certain volume of deionized H<sub>2</sub>O based on the required level 155 of pore volume saturation. Subsequently, the atmospheric gases in the reactor were flushed by 156 purging CH<sub>4</sub> gas at 0.2 MPa at least 10 times. Then, the reactor was submerged in the water-157 ethylene glycol bath i.e. maintained at 303 K, and CH<sub>4</sub> gas pressure was gradually increased to 158 6 MPa. These steady ambient conditions were opted to hinder any hydrate formation. Upon 159 stabilizing the system under these conditions (303 K and 6 MPa), the reactor was cooled to the 160 experimental temperature for initiating the hydrate formation. The hydrate conversion is 161 deemed completed when no significant pressure drop (0.02 MPa in 30 min) was observed. Each 162 experiment in this study was repeated two times.

163 The amount of CH<sub>4</sub> gas consumed during hydrate formation was estimated using the 164 compressibility factor equation of state as shown in (Eq. 1), the normalized gas uptake ( $NG_t$ , 165 Hydrate growth) at any given time t is calculated using (Eq. 2), The percentage of H<sub>2</sub>O to 166 hydrate conversion is determined by (Eq. 3)

167

$$\Delta n_{hyd,t} = V_r \left[ \left( \frac{P}{zRT} \right)_{t=0} - \left( \frac{P}{zRT} \right)_t \right]$$
(Eq. 1)

168

$$NG_t = \frac{\Delta n_{hyd,t}}{n_{H20}} \text{ (moles of CH}_4 / \text{moles of H}_20\text{)}$$
(Eq. 2)

169

$$WtH(\%) = \frac{\Delta n_{hyd,t} \times Hn}{n_{H20}} \times 100$$
 (Eq. 3)

170 where,  $\Delta n_{hyd,t}$  is the moles of CH<sub>4</sub> gas consumed at time t;  $V_r$  is the gas-phase volume within the reactor measured using the helium expansion method[93, 120]; R is the ideal gas constant; 171 172 T and P are the temperature and pressure within the reactor; z is the compressibility of gas 173 calculated using the Pitzer correlation[121];  $n_{H20}$  in (Eq. 2) is the number of moles of H<sub>2</sub>O introduced into the reactor and Hn in (Eq. 3) refers to the hydration number which is defined 174 as the number of H<sub>2</sub>O molecules required to encapsulate one guest (CH<sub>4</sub>) molecule and an ideal 175 hydration number of 5.75 is adapted in this work to comply with other CH<sub>4</sub> hydrate experiments 176 available in the literature[93, 122]. 177

The gas storage capabilities of porous materials were evaluated based on CH<sub>4</sub> capacity relative to the sample's H<sub>2</sub>O content (hydrate storage capacity:  $q_{CH4}^w$ ), and CH<sub>4</sub> capacity relative to the dry mass of the solid (dry weight storage capacity:  $q_{CH4}^A$ ) as shown in (Eq. 4) and (Eq. 5)

$$q_{CH4}^{W}(wt.\%) = \frac{m_{CH4}}{(m_{H20} + m_{CH4})} \times 100$$
 (Eq. 4)

181

$$q_{CH4}^{A}(wt.\%) = \frac{m_{CH4}}{(m_{solid} + m_{CH4})} \times 100$$
 (Eq. 5)

Here,  $m_{H2O}$  and  $m_{solid}$  denote the masses of the H<sub>2</sub>O and dried solid in the reactor, while  $m_{CH4}$ denotes the quantity of enclathrated CH<sub>4</sub> as calculated from (Eq. 1).

Furthermore, another essential representation for industrial application purposes is the CH<sub>4</sub> capacity relative to the total mass of the system (total weight storage capacity:  $q_{CH4}^{T}$ ), which was also evaluated as shown in (Eq. 6)

$$q_{CH4}^{T}(wt.\%) = \frac{m_{CH4}}{m_{tot}} \times 100$$
 (Eq. 6)

187 Here,  $m_{tot}$  refers to the mass of the total system, taking into account the mass of the dried 188 solid, the H<sub>2</sub>O, as well as the enclathrated CH<sub>4</sub>. 189 The rate of CH<sub>4</sub> hydrate formation is calculated using a discrete first-order forward difference
190 method as shown in (Eq. 7).

$$\frac{dN_t}{dt} = \left(\frac{d\Delta n_{hyd}}{dt}\right) = \frac{\Delta n_{hyd,t+\Delta t} - \Delta n_{hyd,t}}{\Delta t}, \Delta t = 0.5 min$$
(Eq. 7)

191

192 3. CH<sub>4</sub> Hydrate kinetics

193 One of the methods for analyzing the hydrate growth is by evaluating the post-induction time 194 data using different reaction models. In this work, the CH<sub>4</sub> uptake upon hydrate formation was studied under isothermal conditions, and the kinetics of hydrate growth (enclathration reaction) 195 196 in the presence of porous media was analyzed with three different kinetic models. The 197 crystallization kinetics of gas hydrates can be adequately explained utilizing the Johnson-Mehl-198 Avrami-Kolmogorow (JMAK) [123-125] model, which assumes the kinetics of isothermal 199 phase transformation from H<sub>2</sub>O/guest gas (CH<sub>4</sub> in this work) to solid-state based on random 200 nucleation with a constant growth rate. This model has previously been applied to investigate 201 hydrate growth kinetics[122, 126-131] and is presented in (Eq. 8)

$$\alpha_{WtH} = 1 - \exp\left(-k(t)^n\right) \tag{Eq. 8}$$

202

203 where,  $\alpha_{WtH}$  is water-to-hydrate conversion ratio at time *t*, *k*, and *n* are 204 formation/crystallization rate constant and Avrami exponent respectively, which can be 205 obtained by fitting the experimental data.

In addition to the JMAK model[125], Lee et al.[132] proposed a kinetic model with two adjustable parameters to investigate hydrate growth in porous media, and the amount of gas consumed during hydrate formation is described as a function of time (Eq. 9)

$$\frac{n_{gas}}{n_{H20}} = \frac{\alpha}{5.75} \left[ 1 - \exp(-5.75K(f_{exp} - f_{eq})t) \right]$$
(Eq. 9)

11

209 where,  $n_{gas}$  is the mole of gas consumed during hydrate formation at the time t,  $n_{H2O}$  is the 210 mole of H<sub>2</sub>O used in the experiment,  $f_{exp}$  and  $f_{eq}$  are the fugacities of gas in the vapor phase 211 (MPa) at the operating thermodynamic conditions and in three-phase equilibrium (MPa), which 212 are obtained from Holley et .al[133]. *K* and  $\alpha$  are the adjustable parameters where *K* is regarded 213 as the overall rate constant (min<sup>-1</sup> MPa<sup>-1</sup>).

While the JMAK model[125] is often used in the literature, and can adequately describe the initial crystallization of hydrates, it is also important to emphasize that the diffusion of guest gas/H<sub>2</sub>O through the hydrate layer is limited or hindered at the latter stage of hydrate growth[134, 135]. Considering this, the hydrate growth kinetics can be described by both primary crystallization and diffusion-controlled secondary crystallization rate by evaluating the experimental data with the reaction model proposed by Hay[136], presented in (Eq. 10)

$$\alpha_{WtH} = \alpha_P (1 - \exp(-k_P t^n))(1 + (k_s t^{0.5}))$$
(Eq. 10)

220 where,  $\alpha_{WtH}$  and  $\alpha_P$  are water-to-hydrate conversion ratio at time t, and at the end of the 221 primary process, respectively.  $k_P$  and  $k_s$  are the rate constant for primary crystallization growth 222 and the rate constant for diffusion-controlled secondary crystallization growth, respectively. n223 is Avrami exponent. Although the model presented in (Eq. 10) is extensively used in polymer 224 crystallization[136-139], it is for the first time adopted for gas hydrates in our work as the model can fundamentally explain the hydrate initial growth based on the JMAK model[125] 225 226 (first term in Eq. 10) and later affected by the diffusion (second term in Eq. 10). More details 227 on the analysis are presented in the results and discussion section.

The performance of these kinetic models in predicting water-to-hydrate conversion was quantified using average absolute deviation (AAD) as shown in (Eq. 11),

$$AAD = \frac{1}{N} \sum_{i=1}^{N} |E_i^{\alpha} - P_i^{\alpha}|$$
(Eq. 11)

12

230  $N, E_i^{\alpha}$  and  $P_i^{\alpha}$  refer to the number of data, experimental and predicted water-to-hydrate 231 conversion respectively.

232

233 4. Results and discussion

234 4.1. Material characterizations

235 SBA-15 C8 and Ring-PMO were subjected to multiple characterizations both pre- and post-236 clathrate formation. The current section presents the characterization of the materials pre-237 clathrate formation and section 4.5 presents material characterizations post-clathrate formation. 238 The investigation of the FT-IR spectra recorded for both materials, as shown in Figure 3, clearly demonstrates the siliceous nature, owing to the broad band around 3400 cm<sup>-1</sup>, together 239 with the prominent peaks at 1100 cm<sup>-1</sup> and 800 cm<sup>-1</sup>, indicating the presence of -OH groups, 240 241 Si-O-Si bonds, and Si-OH species respectively. When comparing the FTIR spectra of pure 242 SBA-15 and the alkyl-chain grafted SBA-15 C8 (Figure S1), a substantial reduction in the Si-OH band at 3750 cm<sup>-1</sup>, as well as the emergence of bands at 2800-3000 cm<sup>-1</sup>, indicates the 243 successful surface modifications with C8 chains. The identical bands at 2800-3000 cm<sup>-1</sup> in the 244 245 Ring-PMO sample also provide evidence of the organic nature of the PMO material.

Upon investigation of the TGA curve, as recorded for the SBA-15 C8 sample (Figure S2), further confirmation of the successful alkyl grafting was concluded. A mass loss of 15.39% between 473 K and 1073 K was observed, originating from the degradation of the surface octyl groups. The grafting density of the C8 chains, expressed in groups per nm<sup>2</sup>, is subsequently calculated using (Eq. 12)

251

Grafting density 
$$\left(\frac{groups}{nm^2}\right) = \frac{\Delta m \times N_A}{M_{group} \times S_{BET}}$$
 (Eq. 12)

where  $\Delta m$  is the weight loss as determined using the TGA curve,  $N_A$  is Avogadro's constant,  $M_{group}$  is the molar mass of the octyl chain and  $S_{BET}$  is the surface area of the SBA-15 material before the surface modification. Ultimately it was determined that the SBA-15 C8 material has a grafting density of  $\approx$  1.2 octyl groups per nm<sup>2</sup>.

256 As shown in Figure 4a, both SBA-15 and SBA-15 C8 materials, as well as Ring-PMO 257 material, exhibit type-IV isotherms with H1 hysteresis which is an archetypical of mesoporous 258 materials with cylindrical pores. Pore size analysis using the BJH methods further confirms the 259 presence of mesoporous in the range of 5 nm and 8 nm for the SBA-15 and Ring-PMO materials respectively (Figure 4b). The Nitrogen uptake at  $P/P^{\circ} > 0.95$  for the SBA-15 samples 260 261 is due to interparticle porosity and is not taken into account in the pore size distribution. For the Ring-PMO there is even a larger nitrogen uptake at  $P/P^{\circ} > 0.95$ . Next to possible 262 interparticle porosity, the Ring-PMO possesses also - next to the hexagonal mesoporous -263 264 larger spherical voids (See TEM image in Figure 6c). Uptake at relative pressures in the region  $P/P^{\circ} = [0.95, 0.99]$  corresponds to voids of 20 - 100 nm. While a high BET surface area of 676 265  $m^2 g^{-1}$  was observed in the case of pure SBA-15, the surface area decreased to 345 m<sup>2</sup> g<sup>-1</sup> upon 266 267 surface grafting of the C8 chains. The aforementioned surface modification also resulted in a decrease from 0.78 cm<sup>3</sup> g<sup>-1</sup> to 0.49 cm<sup>3</sup> g<sup>-1</sup> in total pore volumes. The Ring-PMO material also 268 exhibited high surface area and total pore volume of 849 m<sup>2</sup> g<sup>-1</sup> and 0.99 cm<sup>3</sup> g<sup>-1</sup>. Table 2 269 270 outlines the properties of the hydrophobic porous materials used in this work.

Information on the structural ordering of the materials was determined using XRD and the data is shown in Figure 5. The diffractogram of the SBA-15 C8 material exhibit typical (100), (110), and (200) reflections, confirming the archetypical P6mm symmetry of the hexagonally packed mesopores within the structures. In the case of Ring-PMO a single, slightly broader (100) reflection was observed, indicating a less semi-crystalline ordering compared to the SBA-15 C8 sample.

The materials were also analyzed through TEM to further investigate the particle morphologies, as well as porosities. As can be seen from Figures 6(a) and 6(b), the SBA-15 C8 material is composed of rod-like particles, with mesopores present throughout the material. The same presence of mesopores in the Ring-PMO material is also confirmed in the TEM images (Figures 6(c) and 6(d)). In Figure 6(c) the spherical voids responsible for the increased nitrogen uptake at high P/P°, as discussed above, can be seen. The mesoporous visible in Figure 6(d) are open and not cubic or inkbottle pores, as the isotherm in Figure 3(a) did not show the typical cavitation at P/P° = 0.42, typical for cubic or inkbottle pores.

285

#### 286 4.2. CH<sub>4</sub> consumption and hydrate formation rate

287 CH<sub>4</sub> hydrate formation experiments were conducted at three different temperatures of 269 288 K, 274 K, and 276 K at an initial pressure of 6 MPa. Multiple pore-volume saturations ranging 289 from 70% to 350% were chosen to alter the H<sub>2</sub>O content in SBA-15 C8 and Ring-PMO, which 290 also meets under-saturated/saturated/over-saturation conditions. To ensure consistency, 1 g of 291 SBA-15 C8 and Ring-PMO was used in all the experiments. Table 3. summarizes the 292 experimental conditions, as well as CH<sub>4</sub> hydrate formation results for SBA-15 C8 and Ring-293 PMO. Given that a larger driving force has a favorable correlation with both rate of hydrate 294 formation and induction time (shorter), this works sets the experimental pressure of 6 MPa. 295 Accordingly, the calculated driving force is  $\approx 3.7$  MPa, 3.2 MPa, and 2.7 MPa at 269 K, 274 296 K, and 276 K, respectively, where the equilibrium pressure for CH<sub>4</sub> hydrate is considered as  $\approx$ 297 2.3 MPa, 2.8 MPa, and 3.3 MPa at 269 K, 274 K, and 276 K, respectively[36, 140].

Figures 7(a) and 7(b) show the normalized gas uptake during CH<sub>4</sub> hydrate formation in SBA-15 C8 at 269 K and 274 K with multiple pore-volume saturations, respectively. Figures S3, S4, and S5 show the full-time scale of the experiments at 269 K, 274 K, and 276 K. The hydrate formation being exothermic, a sudden spike in the sample bed temperature (measured by Ktype thermocouple; Testo SE & Co. KGaA) was considered to be the onset of hydrate formation, where the pressure drop observed within the reactor was translated to CH<sub>4</sub> uptake. 304 The time zero in all the Figures corresponds to the onset of hydrate formation/nucleation. As 305 seen in Figures 7 and S4, the CH<sub>4</sub> hydrate formation kinetics in SBA-15 C8 at all the 306 experimental conditions are rapid, where approximately 80% to 90% of the gas uptake occurred 307 within 90 min from nucleation. A bar graph of average storage capacities achieved at 90<sup>th</sup> min 308 is presented in Figure S6. The effect of pore-volume saturation can also be seen in Figure 7 309 where an increase in H<sub>2</sub>O content led to an increase in gas uptake, however, when SBA-15 C8 310 was saturated with 200% of pore-volume which corresponds to 1 g H<sub>2</sub>O, showed a reduced gas 311 uptake compared to 130% pore-volume saturation (0.65 g H<sub>2</sub>O). At 269 K and 274 K, a 312 maximum uptake of 82.9 mmol CH<sub>4</sub>/mol H<sub>2</sub>O and 81.8 mmol CH<sub>4</sub>/mol H<sub>2</sub>O was observed for 313 200% pore-volume saturation, which is approximately 15% and 7% lesser than the CH<sub>4</sub> uptake 314 at 130% pore-volume saturation at the respective temperatures. It is plausible that the CH<sub>4</sub> 315 diffusion/circulation pathways through the pore network could be impeded by this relatively 316 high amount of H<sub>2</sub>O, which would explain the system's considerable reduction in gas uptake 317 when the H<sub>2</sub>O content is higher than the critical value and similar results for optimal H<sub>2</sub>O 318 content in carbon materials were also reported by Celzard et al.[70] and Zhou et al.[141]. This 319 shows that there exists an optimum pore-volume saturation for SBA-15 C8 which is considered 320 to be 130%. These experiments reveal the significance of critical H<sub>2</sub>O content for high gas 321 storage capacities in porous materials. Furthermore, experiments at 276 K (Figure S5) also 322 showed a similar trend as observed at 269 K and 274 K, with higher gas uptake at 130% pore-323 volume saturation (73.5 mmol CH<sub>4</sub>/mol H<sub>2</sub>O) than at 200% pore-volume saturation (72.9 mmol 324 CH<sub>4</sub>/mol H<sub>2</sub>O). As anticipated, the CH<sub>4</sub> uptake decreased with an increase in temperature from 325 269 K to 276 K, which indicates the influence of the driving force, and a similar trend was also 326 observed in porous silica gel particles[54]. However, it is also important to mention that the 327 experiments with 70% and 100% pore-volume saturations at 276 K failed to nucleate despite 328 having a driving force of 2.7 MPa.

329 Figures 8(a) and 8(b) show the average gas uptake during CH<sub>4</sub> hydrate formation at 269 K 330 and 274 K in Ring-PMO with different pore-volume saturations, respectively. Figures S7 and 331 S8 show the full-time scale of experiments at 269 K, and 274 K. Similar to SBA-15 C8, the 332 temperature spikes within the reactor indicated the onset of hydrate formation. In contrast to 333 SBA-15 C8, multiple exothermic peaks within the Ring-PMO bed were observed at the 334 maximum pore-volume saturation used, implying multiple nucleation events and the 335 heterogeneity of hydrate formation and similar observations of multiple temperature spikes in 336 porous materials were also reported in the literature[142-145]. Figure 9 depicts an example of 337 multiple temperature spikes observed in Ring-PMO when saturated to 350% of pore volume. 338 Analogous to SBA-15 C8, Ring-PMO also demonstrated a critical H<sub>2</sub>O content for achieving 339 a maximum CH<sub>4</sub> storage capacity, with 101.2 mmol CH<sub>4</sub>/mol H<sub>2</sub>O when saturated to 200% (2 340 g H<sub>2</sub>O) and 86.7 mmol CH<sub>4</sub>/mol H<sub>2</sub>O when saturated to 350% (3.5 g H<sub>2</sub>O) at 269 K. Despite 341 multiple nucleations, the Ring-PMO at 350% pore-volume saturation showed a lower 342 conversion of H<sub>2</sub>O into hydrates and a similar pattern was also seen at higher temperatures 343 (276 K: Figure S9). Akin to SBA-15 C8, the Ring-PMO failed to nucleate at lower pore-volume 344 saturation of 70% at 274 K and from 70% to 130% pore-volume saturations at 276 K. A 345 maximum duration of 6 hrs. was set for any event of hydrate nucleation or temperature spike 346 within the bed, after which the experiments were discontinued. Figure S6 presents a bar graph of storage capacities achieved at 90<sup>th</sup> min in Ring-PMO at all studied conditions. 347

The average rate of hydrate formation was measured every 0.5 min from the onset of the nucleation point for both SBA-15 C8 and Ring-PMO at all the conditions studied in this work. As can be seen from Figures S10 and S11, the rate of hydrate formation increased with an increase in pore-volume saturation at both temperatures irrespective of the material used. Despite a depreciation in CH<sub>4</sub> uptake, the 200% pore-volume saturation in SBA-15 C8 at 274 K (Figure S10b) and 276 K (Figure S12) showed a steeper peak compared to 130% pore354 volume saturation owing to its relatively high initial gas uptake upon the nucleation event. 355 Rapid hydrate growth can also be seen upon hydrate formation at 269 K, and 274 K for 130% 356 and 200% pore-volume saturated samples followed by a gradual decrease. Similar results were 357 also observed when the temperature was increased by 2 K but at a slower growth rate. On the 358 other hand, the 350% pore-volume saturation in Ring-PMO (Figure S11) at both temperatures 359 showed a lower rate of hydrate formation compared to 200% pore-volume saturation by virtue 360 of its slow gas uptake which is evident from Figure 8. Multiple nucleation events in 350% pore-361 volume saturation can also be seen in Figures S11 and S13 if one plots the average rate of gas 362 hydrate formation as a function of time (50 to 300 min). Similar to SBA-15 C8, a rapid hydrate 363 growth was observed in Ring-PMO samples followed by a gradual decrease, however, 364 increasing the temperature to 276 K decelerated the hydrate growth, as a result of driving force.

365

#### 366 4.3. Comparison of CH<sub>4</sub> hydrate formation in SBA-15 C8 and Ring-PMO

367 In order to compare the performance of SBA-15 C8 and Ring-PMO porous materials in 368 promoting CH<sub>4</sub> hydrate formation and growth, their normalized gas uptake curves at 269 K and 369 274 K are plotted in Figure 10. It is evident from the figure that the CH<sub>4</sub> uptake characteristics 370 of SBA-15 C8 and Ring-PMO are distinctively different even when the driving forces are the same, resulting in a significantly higher gas uptake for SBA-15 C8 compared to Ring-PMO at 371 372 70%, 100%, and 130% pore-volume saturations. However, at 200% pore-volume saturation, 373 the Ring-PMO surpassed the storage capacity compared to SBA-15 C8 (c.f. Table 3) at both 374 temperatures, but it is also important to mention that at such a pore-volume saturation the SBA-375 15 C8 has already demonstrated a drop in gas uptake due to the material's critical H<sub>2</sub>O content, 376 as mentioned in the previous section. Similar results were also observed at 276 K (Figure S14). 377 Considering the time taken for experiments to achieve 90% of maximum storage capacity and 378 eventually obtain a plateau, the hydrate formation in SBA-15 C8 was observed to take a longer period relative to Ring-PMO. For instance, in the case of 130% pore-volume saturation at 274
K, it took approximately 90 min to achieve 90% (47.2 mmol CH<sub>4</sub>/mol H<sub>2</sub>O) of maximum
storage capacity in Ring-PMO (52.4 mmol CH<sub>4</sub>/mol H<sub>2</sub>O) and 82% (72.2 mmol CH<sub>4</sub>/mol H<sub>2</sub>O)
of maximum storage capacity in SBA-15 C8 (88.0 mmol CH<sub>4</sub>/mol H<sub>2</sub>O). A summary of waterto-hydrate conversion in SBA-15 C8 and Ring-PMO is tabulated in Table 3 and Figure 11.

384 As mentioned, optimal clathrate formation conditions differ between the two materials, 385 owing primarily to the amount of H<sub>2</sub>O introduced to the system. Nevertheless, it is also 386 important to compare the CH<sub>4</sub> storage capacities on a weight basis for both materials more 387 closely, as shown in Table 4. Standardizing the amount of H<sub>2</sub>O in the system revealed that 388 Ring-PMO can store  $\approx 1.2$  times more CH<sub>4</sub> than SBA-15 C8, furthermore, it can enclathrate up 389 to  $\approx$  3.2 times more CH<sub>4</sub> per gram of dry material than SBA-15 C8. Although both the materials 390 demonstrated a quick propensity in storing CH<sub>4</sub> as clathrate hydrates, Ring-PMO showed 391 relatively high storage capacity as it can incorporate considerably more H<sub>2</sub>O in the reactor, 392 which translates into substantially increased total dry weight storage capacities. Conclusively, 393 the Ring-PMO has a significantly higher total storage capacity than SBA-15 C8 by a ratio of  $\approx$ 394 2.0 which is of vital importance for future industrial applications.

395 Attempting to compare the performance of porous materials used in this study with other 396 solid CH<sub>4</sub> hydrate promoters could be of potential interest. However, comparing the absolute 397 values hydrate storage capacity  $(q_{CH4}^w)$ , CH<sub>4</sub> capacity relative to the dry mass of the solid  $(q_{CH4}^{A})$ , total weight storage capacity  $(q_{CH4}^{T})$ , water-to hydrate conversion, and hydrate growth 398 399 rate obtained from different laboratories, reactors and methods might not offer the best 400 approach of establishing whether one surpassed the other. For instance, it has been 401 observed[95, 146] that any change in the microstructure (surface roughness) of high-pressure 402 metal reactor will have an immense effect on critical parameters indicated above, and it is also 403 worth noting that the majority of the reactors reported in the literature were made of metal 404 material. However, it is exemplary to make a comparison of total weight CH4 storage capacity 405  $(q_{CH4}^{T})$  and water loading ( $R_{w}$ : mass of H<sub>2</sub>O/mass of solid) as they are essential for industrial 406 application purposes. As shown in Table S1, only works[59, 61, 66, 81, 83, 118, 147-152] 407 using porous materials with  $R_w \leq 2.5$  were chosen for comparison with the material that 408 demonstrated higher  $q_{CH4}^{T}$  in this work. As can be observed, there are quite some materials, 409 particularly at low  $R_w$  that exhibit better CH<sub>4</sub> storage capacity than that reported in this work; 410 nevertheless, it is worth noting that the experimental pressure employed in their study is higher 411 than the pressure used in this work. On the other hand, it should be emphasized that water 412 loading  $(R_w)$  is a significant industrial metric, as cost and mass of solid promoters increases with decrease in  $R_w$ . In this regard, it is important to highlight that Ring-PMO from this work 413 414 is capable of promoting CH<sub>4</sub> hydrate formation at moderate thermodynamic conditions in the 415 mass of water twice its own weight, which could suggest significant cost savings for an 416 industrial application, and this makes the material more appealing than materials that are 417 employed at low water loadings and have higher total storage capacity.

418

419 4.4. Kinetic analysis

420 To investigate the kinetics of hydrate formation at multiple conditions studied in this work, 421 the CH<sub>4</sub> uptake curves were evaluated with different models as described in section 3, and the 422 kinetic analysis was not performed for the materials beyond their critical H<sub>2</sub>O content. Figures 423 S15, S16, S17, and S18 show the predicted kinetic curves from the JMAK model[125], and the 424 regressed values of k and n are presented in Table S2. Given the challenges in visualizing 425 hydrate growth morphology in a porous medium, the Avrami kinetic exponent (n) is commonly 426 utilized in interpreting the geometry (growth dimension) of the hydrate formation and the 427 degree of the crystallization process [123, 124, 153]. Where, n = 3 represents the instantaneous 428 three-dimensional growth of a spherical nucleus, n = 2 represents instantaneous two429 dimensional growth, and n = 1 represents one-dimensional growth. But, as shown in Table S2, 430 the regressed exponent values (n) for the entire growth period are less than 1 for all conditions, 431 inferring instantaneous one-dimensional crystal growth followed by a decrease in hydrate 432 nucleation and growth rates that could be attributed to the mass transfer resistance. Similar low 433 exponent values were also reported by Susilo et al.[127], Luzi et al.[126], Silva et al.[154]. The 434 corresponding AAD values are presented in Table 6. The model proposed by Lee et al.[132] 435 was also used to analyze the kinetics of hydrate growth and the corresponding kinetic curves 436 are presented in Figures S19, S20, S21, and S22, together with the regressed values in Table 437 S2. As can be seen, Lee et al.[132] model predicted the initial kinetics of hydrate growth better 438 than the JMAK model[125], nevertheless, later in time it reached a plateau and was unable to 439 provide a close fit. This was also reflected in the AAD values (Table 6), where the maximum 440 deviation in model prediction was determined at a later stage due to the presence of the 441 adjustable parameter ( $\alpha$ ); suggesting the crystallization growth will eventually approach a 442 constant. However, the real-time data demonstrated not only an exponential increase at first 443 but also continuous growth with a reduced rate thereafter as the mass transfer (guest gas  $/H_2O$ ) 444 dominates crystallization in the porous medium. Conclusively, the predictive power of both 445 JMAK[125] and Lee et al.[132] models revealed limitations in evaluating the hydrate growth 446 at both the reaction-controlled and the diffusion-controlled regimes, resulting in a large 447 deviation from the real-time data either at the beginning or later stages of the growth kinetics. 448 Given the limitations of single-step kinetic models, it is preferable to have an integrated 449 multistep model to obtain a more accurate representation of the hydrate kinetics. Consequently, 450 the model proposed by Hay[136] has been adapted in this work for evaluating the hydrate 451 growth kinetics at both the reaction-controlled (primary growth stage) and the diffusion-452 controlled regimes (secondary growth stage). A more detailed version of Hay's model is 453 presented in their earlier work on crystallization kinetics [136, 139, 155]. As can be seen from

454 (Eq. 10), the total water-to-hydrate conversion  $\alpha_{WtH}$  can be classified into water-to-hydrate 455 conversion in the primary and secondary growth stage as shown in (Eq. 13)

$$\alpha_{WtH} = \alpha_{WtH,P} + \alpha_{WtH,S} \tag{Eq. 13}$$

456 The primary growth stage, which is attributed to the nucleation and rapid hydrate growth was 457 analyzed using the JMAK model[125] (Eq. 14), assuming that it ends before the onset of the 458 secondary growth stage ( $\alpha_P$ ), i.e. the diffusion-controlled regime.

$$\alpha_{WtH,P} = \alpha_P (1 - \exp(-k_p t^n))$$
(Eq. 14)

459 The  $k_p$  and n are the same as described in (Eq. 10), and applying double logarithm, (Eq. 14) 460 can be rewritten as presented in (Eq. 15)

$$\ln\left(-\ln\left(1-\alpha_{WtH,P}/\alpha_{P}\right)\right) = nln(t) + ln(k_{P})$$
(Eq. 15)

In this analysis,  $\alpha_p$  was used as an adjustable parameter and its value was chosen from the best linear fit of the data to (Eq. 15) as determined by  $R^2$  (for Ring-PMO at 276 K: Figure 12 and the corresponding value of  $ln(k_p)$  was determined from the intercept (Figures S23 and S24). In every case, the exponent n value was set to 1 assuming one-dimensional growth. The waterto-hydrate conversion in the second stage is defined as shown in (Eq. 16)

$$\alpha_{WtH,S} = \alpha_{WtH,P}(k_s t^{0.5}) \tag{Eq. 16}$$

466 Substituting (Eq. 16) and (Eq. 14) in (Eq. 13) results in the overall kinetic model as presented in (Eq. 10). The kinetic rate constant for the secondary growth or crystallization stage was 467 obtained from the slope of the linear fit by plotting  $\left[\left(\frac{\alpha_{WtH}-\alpha_P}{\alpha_P}\right)\right]$  vs  $t^{0.5}$  (Figures S25 and S26). 468 The corresponding rate constants  $k_P$ ,  $k_s$  and  $\alpha_P$  for all the experiments performed in this work 469 470 are presented in Table 5. As shown in Table 5, the secondary kinetic rate constant  $(k_s)$ , curtails 471 to a lower value after the first stage of growth in both SBA-15 C8 and Ring-PMO irrespective 472 of the driving force applied and this can be attributed to slower conversion rates due to mass 473 transfer resistance in these porous mediums upon achieving certain water-to-hydrate 474 conversion. As already mentioned above, the multistage kinetic model showed better 475 predictions in the hydrate kinetics (Figures 13, 14, S27, S28) compared to the predictions from 476 the JMAK[125] and Lee et al.[132] models, which is further highlighted in AAD values (Table 477 6). The contribution of primary and secondary-stage hydrate growth on water-to-hydrate 478 conversion can also be extracted from this multistage model; for instance, the secondary stage 479 contributes about 23% to the overall water-to-hydrate conversion for 200% pore-volume 480 saturated Ring-PMO at 276 K as shown in Figure 15.

481 Subsequently, the model with the lowest AAD from the real-time data was used to determine 482 the apparent activation energy of CH<sub>4</sub> hydrate formation using the Arrhenius equation (Eq. 17) 483 for the pore-volume saturations with the maximum CH<sub>4</sub> storage capacity.

$$k = A * \exp\left(-\frac{E_a}{RT}\right)$$
(Eq. 17)

A is the frequency factor (min<sup>-1</sup>),  $E_a$  is the activation energy (J.mol<sup>-1</sup>), T is the temperature in 484 (K), R is the gas constant (8.314 J.K<sup>-1</sup>.mol<sup>-1</sup>) and k is the rate constant, which corresponds to 485  $k_p$  from (Eq. 10). The least-squares linear fit for 130% pore-volume saturation in SBA-15 C8 486 and 200% pore-volume saturation in Ring-PMO gave apparent activation energy,  $E_a$  of -79 487 kJ.mol<sup>-1</sup> and -124 kJ.mol<sup>-1</sup>, respectively as shown in Figure 16. One of the frequently observed 488 489 characteristics of hydrate formation is its large negative activation energy, which was also 490 previously reported for the sI CH<sub>4</sub> hydrates[19, 156], sII propane hydrates[157], Di and 491 trifluoromethane hydrates[158, 159], and sII THF-Argon hydrates[160]. Chen et al.[161] 492 described this anti-Arrhenius behavior for CH<sub>4</sub> hydrates by hypothesizing that hydrate 493 formation reaction (in the primary stage) proceeds faster at lower temperatures resulting in a 494 higher yield of hydrate in a given time. However, no activation energy value was reported by them. An apparent activation energy value of -106 kJ.mol<sup>-1</sup> and -94 kJ.mol<sup>-1</sup> for CH<sub>4</sub> hydrates 495 496 was reported by Vysniauskas and Bishnoi[19] and Kitamjima et al.[156], respectively. Most 497 explanations on the crystallization kinetics exhibiting negative activation energy hypothesize

498 the competitive influence between crystal growth and nucleation[19, 162, 163]; however, the 499 most likely interpretation of this anti-Arrhenius trend or negative activation energy can be 500 linked to free energy change as a function of cluster size based on the theory of nucleation with 501 special properties of H<sub>2</sub>O clathrates as explained by Barrer and Ruzicka[160], where the energy 502 barrier for enclathration decreases with decreasing temperature and simultaneously small 503 cluster sizes reaches criticality followed by an increased rate of nucleation. Furthermore, 504 hydrate formation being a physical reaction, the energies involved in reorganization/clustering 505 of H<sub>2</sub>O molecules and interactions between H<sub>2</sub>O-CH<sub>4</sub> are reported to be approximately between (-47 kJ.mol<sup>-1</sup> to -50 kJ.mol<sup>-1</sup>)[164-168] and (-17 to -19 kJ.mol<sup>-1</sup>)[169, 170] respectively, and 506 the maximum sum of  $\approx$  -70 kJ.mol<sup>-1</sup> supports the negative activation energies calculated in this 507 508 work. In addition, these negative apparent activation energy highlights the curve-fitting nature 509 of these models.

510

#### 511 4.5. Characterization of SBA-15 C8/Ring-PMO post-hydrate formation

512 To evaluate the material's resilience towards hydrate growth, multiple characterization 513 methods were used to investigate any chemical or morphological alterations post-clathrate 514 formation. The FTIR spectra of SBA-15 C8 and Ring-PMO, presented in Figure 17, reveal no 515 significant differences from fresh materials (pre-clathrate condition), showing that no chemical 516 modification of the materials takes place. Similarly, the effect of the clathrate formation process 517 on the porosity of the materials was investigated by N<sub>2</sub> sorption, and the results are shown in Figures 18(a) and 18(b). Upon careful analysis of the N<sub>2</sub> sorption isotherms of the SBA-15 C8 518 materials, only minor alterations in terms of surface areas (345 vs 325 m<sup>2</sup> g<sup>-1</sup>) and total pore 519 volumes (0.49 vs 0.46 cm<sup>3</sup> g<sup>-1</sup>) were observed upon being exposed to the clathrate formation 520 process. However, Ring-PMO has shown slightly more noticeable changes in the total pore 521 volume (0.99 vs 0.90 cm<sup>3</sup> g<sup>-1</sup>) and BET surface area (849 vs 747 m<sup>2</sup> g<sup>-1</sup>). In general, it can be 522

523 concluded that the materials lose fairly small but not substantial porosities upon clathrate 524 formation, highlighting their viability as clathrate hydrate promoters for longer and multiple 525 cycles. The XRD diffractograms of both the material's pre- and post-clathrate formation, as 526 shown in Figure 19, clearly indicate the conservation of structural parameters upon being 527 subjected to the clathrate formation conditions. Furthermore, the TEM images of SBA-15 C8 528 and Ring-PMO showed no morphological changes (Figure 20) post-clathrate formation. Close 529 inspection of the images demonstrates the retention of the mesoporous channels within the 530 materials, indicating the preservation of the porous structures throughout the clathrate 531 formation process.

532

533 5. Conclusion

534 CH<sub>4</sub> hydrate formation and growth in the presence of mesoporous hydrophobic materials 535 (SBA-15 C8 and Ring-PMO) was investigated at multiple pore-volume saturations and 536 temperatures; (269 K, 274 K, and 276 K) with an experimental pressure of 6 MPa. The kinetic 537 parameters, such as maximum gas uptake and water-to-hydrate conversion, were observed for 538 both materials at the lowest temperature. A rapid hydrate growth was demonstrated by both 539 materials, which is favorable for CH<sub>4</sub> storage applications. Nevertheless, SBA-15 C8 exhibited 540 a relatively longer time than Ring-PMO to attain its maximum storage capacity irrespective of 541 the driving force applied. An optimal pore-volume saturation of 130% for SBA-15 C8 and 542 200% for Ring-PMO was identified, beyond which a considerable depression in gas uptake 543 was observed. At 269 K, a maximum storage capacity of 98.2 mmol CH<sub>4</sub>/mol H<sub>2</sub>O at 130% 544 pore-volume saturation and 101.2 mmol CH<sub>4</sub>/mol H<sub>2</sub>O at 200% pore-volume saturation was 545 determined for SBA-15 C8 and Ring-PMO, respectively. At these optimal pore-volume 546 saturations, it was also found that the Ring-PMO material could store up to  $\approx 3.2$  times more 547 CH<sub>4</sub> in the form of clathrate per gram of dry solid, compared to the SBA-15 C8 material.

548 Furthermore, the Ring-PMO displayed a total storage capacity of 6.5 wt.%, a factor  $\approx 2.0$  times 549 higher compared to the SBA-15 C8 material. Three different models were used for kinetic 550 modeling of CH<sub>4</sub> hydrate formation and growth in both the materials under all driving forces 551 and pore-volume saturations. A multistage kinetic model performed significantly better in 552 predicting the experimental data (water-to-hydrate conversion), with a low average absolute 553 deviation (AAD). The apparent activation energy values for SBA-15 C8 and Ring-PMO were 554 extracted from the best-fit kinetic model at 130% and 200% pore-volume saturation, 555 respectively. Both materials demonstrated an inverse temperature dependence on the reaction rates, owing to negative apparent activation energy (-79 kJ.mol<sup>-1</sup>: SBA-15 C8, -124 kJ.mol<sup>-1</sup>: 556 557 Ring-PMO) which are also comparable with the values reported in the literature. Finally, no 558 morphological change was observed for both materials after many cycles of hydrate formation, 559 confirming the preservation of structural integrity. The results from this study conclude that 560 the tailored hydrophobic porous materials; SBA-15 C8 and Ring-PMO are suitable for 561 promoting CH<sub>4</sub> hydrate growth and are capable of overcoming the slow kinetics of typical CH<sub>4</sub> 562 formation, paving the way for efficient storage and transportation.

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579 Supplementary data

- 580 The supplementary data to this article can be found online at:
- 581

582

583

# **Table 1.** Chemicals description

Source
ChemLab
ChemLab
ChemLab
Merck Life Science
Sigma Aldrich
Fisher Scientific
Gelest
Gelest

# **Table 2.** Properties of materials used in this work

	SBA-15	SBA-15 C8	Ring-PMO	
$S_{BET} (m^2 g^{-1})$	676	345	849	
$V_{tot} (cm^3 g^{-1})^a$	0.78	0.49	0.99	
Pore size (nm) <sup>b</sup>	5.5	4.7	8.0	
<sup>a</sup> Determined at a relative pressure of 0.95 <sup>b</sup> Determined using the BJH method on the desorption branch				

	D	T	SBA-15 C8		Ring-Pl	MO
Condition	(MPa)	(K)	NG <sub>t</sub> (mmol CH <sub>4</sub> /mol H <sub>2</sub> O)	WtH (%)	NGt (mmol CH4/mol H2O)	WtH (%)
70% pore-volume sat.	6	269	55.0	31.6	25.2	14.5
100% pore-volume sat.	6	269	69.0	39.7	49.7	28.6
130% pore-volume sat.	6	269	98.2	56.5	69.1	39.7
200% pore-volume sat.	6	269	82.9	47.7	101.2	58.2
350% pore-volume sat.	6	269	-	-	86.7	49.8
70% pore-volume sat.	6	274	39.7	22.8	N/H	N/H
100% pore-volume sat.	6	274	55.6	32.0	29.5	17.0
130% pore-volume sat.	6	274	88.0	50.6	52.4	30.1
200% pore-volume sat.	6	274	81.8	47.0	85.9	49.4
350% pore-volume sat.	6	274	-	-	78.9	45.4
70% pore-volume sat.	6	276	N/H	N/H	N/H	N/H
100% pore-volume sat.	6	276	N/H	N/H	N/H	N/H
130% pore-volume sat.	6	276	73.5	42.4	N/H	N/H
200% pore-volume sat.	6	276	72.9	41.9	75.5	43.4
350% pore-volume sat.	6	276	-	-	67.4	38.7

N/H: no hydrates observed, '- ': no experiments performed

**Table 4.** Comparison of the hydrate storage capacity  $(q_{CH4}^w)$ , dry weight storage capacity  $(q_{CH4}^A)$  and total storage capacity  $(q_{CH4}^T)$  of both the materials, as determined at 269 K and 6 MPa.

	$q^w_{CH4}( ext{wt.}\%)$	q^A_{CH4}(wt.%)	$q_{CH4}^{T}($ wt. % $)$	
SBA-15 C8	8.0	5.4	3.3	
Ring-PMO	9.4	17.2	6.5	
<sup>a</sup> Determined at pore volume saturation of 130%				
<sup>b</sup> Determined at pore volume saturation of 200%				

**Table 5.** Regressed values of rate constants  $(k_P, k_S)$ ,  $(\alpha_P)$  for Hay model[136] analyzed in this work.

			Hay[13	6]	
SBA-15 C8	T (K)	$lpha_p$	$k_p (\min^{-1})$	$k_s$ (min <sup>-1</sup> )	
70% pore-volume sat.	269	0.23	1.06E-01	2.56E-02	
100% pore-volume sat.	269	0.27	1.67E-01	3.37E-02	
130% pore-volume sat.	269	0.42	2.12E-01	2.03E-02	
70% pore-volume sat.	274	0.09	1.08E-01	1.03E-01	
100% pore-volume sat.	274	0.19	7.23E-02	3.56E-02	
130% pore-volume sat.	274	0.35	9.41E-02	2.26E-02	
130% pore-volume sat.	276	0.29	9.31E-02	3.10E-02	
			Hay[136]		
Ring-PMO	T (K)	α <sub>p</sub>	$k_p (\min^{-1})$	$k_s$ (min <sup>-1</sup> )	
70% pore-volume sat.	269	0.1	1.23E-01	3.75E-02	
100% pore-volume sat.	269	0.26	1.40E-01	9.72E-03	
130% pore-volume sat.	269	0.36	1.29E-01	7.06E-03	
200% pore-volume sat.	269	0.54	1.27E-01	3.70E-03	
100% pore-volume sat.	274	0.14	6.57E-02	1.32E-02	
130% pore-volume sat.	274	0.23	7.00E-02	1.71E-02	
200% pore-volume sat.	274	0.43	6.82E-02	6.78E-03	
200% pore-volume sat.	276	0.35	2.71E-02	1.04E-02	

## **Table 6.** The AAD values from JMAK[125], Lee et al.[132], and Hay[136] models in

		JMAK[125]	Lee et al.[132]	Hay[136]
SBA-15 C8	T (K)	AAD	AAD	AAD
70% pore-volume sat.	269	1.1	1.1	0.7
100% pore-volume sat.	269	1.2	1.6	0.5
130% pore-volume sat.	269	1.0	2.5	0.6
70% pore-volume sat.	274	0.5	0.7	0.7
100% pore-volume sat.	274	0.9	1.3	0.6
130% pore-volume sat.	274	1.1	2.2	0.9
130% pore-volume sat.	276	1.3	1.4	1.1
				1
		JMAK[125]	Lee et al.[132]	Hay[136]
Ring-PMO	T (K)	JMAK[125] AAD	Lee et al.[132] AAD	Hay[136] AAD
Ring-PMO 70% pore-volume sat.	T (K) 269	JMAK[125] AAD 0.7	Lee et al.[132] AAD 0.4	Hay[136] AAD 0.3
Ring-PMO 70% pore-volume sat. 100% pore-volume sat.	T (K) 269 269	JMAK[125] AAD 0.7 2.2	Lee et al.[132]           AAD           0.4           0.3	Hay[136] AAD 0.3 0.4
Ring-PMO 70% pore-volume sat. 100% pore-volume sat. 130% pore-volume sat.	T (K) 269 269 269	JMAK[125] AAD 0.7 2.2 2.1	Lee et al.[132]         AAD         0.4         0.3         0.5	Hay[136] AAD 0.3 0.4 0.3
Ring-PMO 70% pore-volume sat. 100% pore-volume sat. 130% pore-volume sat. 200% pore-volume sat.	T (K) 269 269 269 269 269	JMAK[125] AAD 0.7 2.2 2.1 1.9	Lee et al.[132] AAD 0.4 0.3 0.5 0.8	Hay[136] AAD 0.3 0.4 0.3 0.2
Ring-PMO 70% pore-volume sat. 100% pore-volume sat. 130% pore-volume sat. 200% pore-volume sat. 100% pore-volume sat.	T (K) 269 269 269 269 269 274	JMAK[125] AAD 0.7 2.2 2.1 1.9 1.2	Lee et al.[132] AAD 0.4 0.3 0.5 0.8 0.2	Hay[136] AAD 0.3 0.4 0.3 0.2 0.3
Ring-PMO 70% pore-volume sat. 100% pore-volume sat. 130% pore-volume sat. 200% pore-volume sat. 100% pore-volume sat. 130% pore-volume sat.	T (K) 269 269 269 269 269 274 274	JMAK[125] AAD 0.7 2.2 2.1 1.9 1.2 1.5	Lee et al.[132] AAD 0.4 0.3 0.5 0.8 0.2 0.7	Hay[136] AAD 0.3 0.4 0.3 0.2 0.3 0.3
Ring-PMO 70% pore-volume sat. 100% pore-volume sat. 130% pore-volume sat. 200% pore-volume sat. 100% pore-volume sat. 130% pore-volume sat. 200% pore-volume sat.	T (K) 269 269 269 269 274 274 274	JMAK[125] AAD 0.7 2.2 2.1 1.9 1.2 1.5 2.4	Lee et al.[132] AAD 0.4 0.3 0.5 0.8 0.2 0.7 0.8	Hay[136] AAD 0.3 0.4 0.3 0.2 0.3 0.3 0.2

predicting water-to-hydrate conversion in all the systems studied in this work



Figure 1. Chemical representation of both Ring-PMO (A) and SBA-15 C8 (B)



**Figure 2.** The schematic of the experimental setup for the study of CH<sub>4</sub> hydrate formation in SBA-15 C8 and Ring-PMO



**Figure 3.** FT-IR recorded transmittance of both SBA-15 C8 (dotted line) and Ring-PMO (solid line) materials



**Figure 4.** N<sub>2</sub> sorption isotherms (a) and corresponding pore sizes (b) of the SBA-15 materials pre- and post- alkyl modification together with N<sub>2</sub> isotherm of Ring-PMO



**Figure 5.** Overview of normalized XRD diffractograms of both SBA-15 C8 (dotted line) and Ring-PMO (solid line) materials



Figure 6. TEM images of the as-synthesized SBA-15 C8 (a and b) and Ring-PMO (c and d) materials



**Figure 7.** Normalized CH<sub>4</sub> uptake profiles during hydrate formation experiments conducted at 269 K (a) and 274 K (b) in SBA-15 C8 at multiple pore-volume saturations. Time zero corresponds to the nucleation point



**Figure 8.** Normalized  $CH_4$  uptake profiles during hydrate formation experiments conducted at 269 K (a) and 274 K (b) in Ring-PMO at multiple pore-volume saturations. Time zero corresponds to the nucleation point



**Figure 9.** Multiple temperature spikes observed in Ring-PMO during CH<sub>4</sub> hydrate formation when saturated to 350% of pore-volume at 274 K



**Figure 10.** Comparison of CH<sub>4</sub> uptake behavior in SBA-15 C8 and Ring-PMO at 269 K (a) and 274 K (b) at multiple pore-volume saturations



Figure 11. Water-to-hydrate conversion (%) in SBA-15 C8 and Ring-PMO at multiple operating conditions



**Figure 12.** Effect of changing  $\alpha_P$  on the degree of fit for 200% pore-volume saturation in Ring-PMO at 276 K



**Figure 13.** Comparing the Hay[136] model to experimental data for water-to-hydrate conversion (%) in SBA-15 C8 at 269 K (a) and 274 K (b)



**Figure 14.** Comparing the Hay[136] model to experimental data for water-to-hydrate conversion (%) in Ring-PMO at 269 K (a) and 274 K (b)



**Figure 15.** The contribution of primary and secondary-stage hydrate growth on water-tohydrate conversion in 200% pore-volume saturated Ring-PMO at 276 K



**Figure 16.** Arrhenius plots for (a) 130% pore-volume saturation: SBA-15 C8, (b) 200% pore-volume saturation: Ring-PMO



**Figure 17.** FT-IR recorded transmittance of both SBA-15 C8 (a) and Ring-PMO (b) materials pre- and post-clathrate formation



**Figure 18.** N<sub>2</sub> sorption isotherms (a) and corresponding pore sizes (b) of the SBA-15 C8 and Ring-PMO materials pre- and post-clathrate formation



**Figure 19.** Overview of the normalized XRD diffractograms of both SBA-15 C8 (a) and Ring-PMO (b) materials pre- and post-clathrate formation, demonstrating the preservation of the structural parameters of both materials upon being exposed to clathrate formation



**Figure 20.** TEM images of pre-(fresh) and post-(used) clathrate formation in SBA-15 C8 (a and b respectively) and Ring-PMO (c and d respectively)

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