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1 Experimental and computational aerodynamic characterisation of 2 urban trees

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9 ABSTRACT

10 The Darcy-Forchheimer method is used for modelling the airflow through vegetation. Seven tree and shrub
11 species with contrasting leaf morphologies were installed in a wind tunnel to allow pressure loss
12 measurements across the plant section. Aerodynamic parameters derived from this experiment were
13 inserted into a COMSOL Multiphysics computational fluid dynamics model. The model was confirmed to
14 be a good predictor for airflow through vegetation ($R^2 = 0.98$), regardless of plant morphology. Moreover,
15 supplementing these data with results from a previous study (which considered herbaceous species)
16 revealed a pattern of pressure loss data, that was already been normalised for plant area density. Although
17 we propose further research into kinetic energy transfer in vegetation, this study provides sufficient
18 interesting information for further applications and modelling to describe and predict urban ecology.

19 NOMENCLATURE

A	Area	m^2
FLS	Functional leaf size	(-)
K	Permeability	m^2
K_1	Inertial permeability	m
LAD	Leaf area density	$m^2 m^{-3}$
LDI	Leaf dissection index	(-)
LS	Leaf size	m^2
M	Mass	kg
P	Perimeter	m
PAD	Plant area density	$m^2 m^{-3}$
Q	Flow rate	$m^3 s^{-1}$
R^2	Coefficient of determination	(-)
SLA	Specific leaf area	$m^2 kg^{-1}$
q	Flux	$m s^{-1}$
v	Fluid velocity	$m s^{-1}$
V	Volume	m^3
ΔP	Pressure loss	Pa
ΔP_{norm}	Normalised pressure loss	(-)
Δx	Distance	m
ρ	Density	$kg m^{-3}$
ϕ	Porosity	(-)
τ	Kendall rank correlation coefficient	(-)
μ	Viscosity	Pa s

20

21 1 INTRODUCTION

22 Describing how air flows through vegetation has been proven to be challenging. However, this knowledge
23 is indispensable in order to evaluate complex processes performed by plants such as particulate matter
24 (PM) mitigation (Beckett et al. 1998; Nowak et al. 2006; Litschike & Kuttler 2008; Pugh et al. 2012; Samson
25 et al. in Pearlmutter et al. 2017) and cooling effects. Furthermore, urban green infrastructure has other
26 important functions; e.g. carbon sequestration (Tallis et al., 2015), improvement of biodiversity
27 (Oberndorfer et al., 2007); water purification and management (Pearlmutter et al., 2017) and human
28 wellbeing (Hartig, Mitchell, Vries, & Frumkin, 2014).

29 Parameterisation of aerodynamic effects of vegetation can be approached in different ways, as discussed
30 in the review of Buccolieri et al. (2018). For example, Buccolieri et al. (2009) and Jeanjean et al. (2016) use
31 a pressure loss coefficient λ which accounts for the ratio of the static pressure difference between the
32 front and the back of the porous medium, and the dynamic pressure (ρv^2) divided by the stream wise
33 length of the material. In contrast, Koch, Samson, & Denys (2019) used the pressure drop normalized for
34 vegetation density, wind speed and length of the material as a measure of how easily air flows throughout
35 a certain vegetation stand. Because of different approaches involved, comparisons between studies are
36 often difficult (Janhäll, 2015).

37 Aerodynamic studies of trees have often involved synthetic simulators, wire constructions or other porous
38 media (Buccolieri et al. 2009; Endalew et al. 2009; Gromke & Ruck 2012); only a few studies have used real
39 trees or branches (Molina-Aiz et al. 2006; Lin & Khlystov 2012; Sase, Kacira, Boulard, & Okushima, 2012;
40 Huang et al. 2013). Moreover, several modelling approaches have been performed, which include
41 numerical airflow models (Connell, Endalew, & Verboven, 2011; De Maerschack, Maiheu, Janssen, &
42 Vankerkom, 2010; Endalew et al., 2009; Hong et al., 2012) or empirical models (Raupach, Woods, Dorr,
43 Leys, & Cleugh, 2001; Tiwary, Morvan, & Colls, 2005; M. Lin, Katul, & Khlystov, 2012b). In all of these
44 approaches, be they experimental or modelling, simplifications are made for the sake of convenience.
45 According to Janhäll (2015), this downscaling of vegetation increases the uncertainty of the results. Also,
46 for trees, Jeanjean et al. (2016) have found that aerodynamic effects are more important for PM mitigation
47 than the deposition processes themselves. This highlights the importance of aerodynamic assessment of
48 vegetation and trees in particular.

49 In our earlier work, Koch et al. (2019), a Darcy-Forchheimer approach was proposed as a model to describe
50 pressure drop over several contrasting herbaceous plant species which were considered as porous media.
51 The Darcy-Forchheimer equation is an extension of the simple Darcy equation, which relates the pressure
52 drop observed when a fluid flows through a porous medium to the flow rate of the fluid. The Forchheimer-
53 drag includes inertial effects that occur at high flow rates. Freshly cut vegetation was brought into a wind
54 tunnel setup, while pressure data results were validated in a COMSOL Multiphysics CFD (Computational
55 Fluid Dynamics) model. Close agreement was found between experimental and modelled data, which
56 suggests Darcy-Forchheimer as a useful approach to aerodynamically characterize different plant species
57 for green wall applications. Furthermore, a classification of species was made in terms of their normalised
58 pressure drop. In this paper, this approach is expanded by assessing its applicability on woody plant
59 species. Trees and shrubs are important forms of urban green infrastructure and are different from green
60 walls in terms of their woody mass. Leaves of trees and shrubs are growing on branches instead of on non-
61 woody stems as with herbaceous species.

62 The objectives of this research are (1) to observe if the Darcy-Forchheimer approach is applicable for
 63 multiple types of vegetation; (2) to investigate potential differences between species in aerodynamic
 64 properties and to compare them with herbaceous outcomes; and (3) to examine if pressure losses over
 65 woody species can be predicted by their leaf morphology.

66








67 2 MATERIALS & METHODS

68 2.1 SPECIES SELECTION AND MORPHOLOGICAL PARAMETERS

69 Species were selected with the aim of covering a broad variety in leaf morphology. Five deciduous as well
 70 as two coniferous tree and shrub species, which are commonly found in Western Europe, were used (Table
 71 1). Tree and shrub specimens were grown in a common garden at Groenenborger Campus of Antwerp
 72 University, Belgium. For this research, plants were selected from the same experimental setup that was
 73 used as in Muhammad, Wuyts, & Samson (2019). The plants were three years old at the time of sampling.
 74 Branches with leaves were sampled between October 2017 and January 2018. For practical reasons only
 75 one-year old branches were collected of the deciduous species. Following the method of Koch et al. (2019)
 76 a series of directly measurable leaf morphological parameters was assessed in order to describe the
 77 selected species on plant and leaf level. Parameters and calculations are given in Table 2.

78

79 Table 1: Selected species. Scientific name and largest measured length and width of an individual leaf or
 80 needle are given. "Largest" means the maximum measured length of a leaf out of all the measured leaves
 81 for the considered plant species.

<i>Catalpa bignonioides</i> Length x width: 200 x 150 mm	<i>Buddleja davidii</i> Length x width: 140 x 60 mm	<i>Betula pendula</i> Length x width: 40 x 60 mm	<i>Carpinus betulus</i> Length x width: 85 x 45 mm
			
<i>Ligustrum ovalifolium</i> Length x width: 45 x 20 mm	<i>Thuja plicata</i> Length x width: 25 x 3 mm	<i>Abies fraserii</i> Length x width: 20 x 3 mm	
			

82

83

84 Table 2: Morphological canopy and leaf parameters determined on the selected tree species. V_{total} : total
 85 volume of the system, V_{plant} : volume of the foliage, A_{leaf} : total area of all the leaves, A_{plant} : area of the entire
 86 plant (leaves and stem/branches), P : leaf perimeter (m), M : dry leaf mass (kg). Circle is the largest circle
 87 that can be drawn onto a leaf.

Parameter	Formula	Unit
Plant Area Density (PAD)	$PAD = \frac{A_{plant}}{V_{total}}$	$m^2 m^{-3}$
Porosity (φ)	$\varphi = 1 - \left(\frac{V_{plant}}{V_{total}}\right)$	dimensionless
Specific Leaf Area (SLA)	$SLA = \frac{A_{leaf}}{M_{leaf}}$	$m^2 kg^{-1}$
Leaf Dissection Index (LDI)	$LDI = \frac{P_{leaf}}{\sqrt{A_{leaf}}}$	dimensionless
Functional Leaf Size (FLS)	$FLS = \frac{A_{circle}}{A_{leaf}}$	dimensionless
Leaf Size (LS)	A_{leaf}	m^2

88

89 2.2 AERODYNAMIC PARAMETERS

90 Permeability, Forchheimer-drag and porosity are the parameters which are used in this study to define air
 91 flow through a porous medium and are derived from wind tunnel experiments. The permeability of a
 92 porous material is its ability to allow a fluid to pass through it and it is closely related to its structure and
 93 porosity. Porosity is a fraction of the volume of voids over the total volume, ranging between 0 (full) and
 94 1 (empty). The Forchheimer-drag coefficient accounts for the kinetic energy and inertia of the fluid and
 95 the typical non-linear relation of fluid flow rate and the pressure drop (Mattis *et al.* 2012). The value of
 96 PAD and porosity, defined in Table 2, varies depending on the packing density (even for a certain species),
 97 which makes a statistical correlation analysis possible.

98 In order to obtain pressure loss (ΔP) data, wind tunnel experiments were performed according to the
 99 method used in Koch *et al.* (2019). A closed circuit wind tunnel with a total length of 6m (2m in length, 1m
 100 wide) was used with an interior fan and had an inner diameter of 103 mm (Fig. 1). On the long side there
 101 was a removable plant compartment with inner diameter 114 mm. The step change in diameter was
 102 considered in the model. Furthermore, the measured pressures and velocities were compared with model
 103 values at corresponding locations. For each wind tunnel run, the wind tunnel fan was used in three
 104 different settings; maximum (a), median (b) and minimum power (c). For each setting fan curves were
 105 derived from pressure versus flow rate values and used as a single boundary condition in the model (see
 106 further). Air velocity data was retrieved with a hot wire anemometer (CTV 110, KIMO Instruments, Chevy-
 107 Cossigny, France), which was placed ± 150 mm in front of the plant compartment. Because wind speed
 108 could only be measured at one point at a time, prior to experiment execution (thus without vegetation),
 109 measurements were taken at three distances (50 mm, 25 mm and at the duct wall) from the duct wall so
 110 that average velocity could be calculated by integrating the wind profile measurements over the flow cross
 111 section. All further calculations were performed with integrated velocity data. Branches of the selected
 112 species were brought into the plant compartment as homogeneously as possible and pressure loss over
 113 the vegetation (branches with leaves attached) was derived by a Pressure Module (750PD2, FLUKE

114 Corporation, Gent, Belgium) with a range of ± 7 kPa and an uncertainty of 0.15%, and a Pressure Calibrator
 115 (717 30G, FLUKE Corporation, Gent, Belgium). Per tree species 6 to 8 samples with different PAD's (plant
 116 area density, Fig. 2 left panel) and corresponding porosities (Fig. 2 right panel) were examined under the
 117 three fan settings (a, b and c). Empty wind tunnel runs were performed as a reference.

118 Pressure loss data was used for calculation of permeability (K) [m^2] and Forchheimer-drag ($\frac{\rho}{K_1}$) [kg m^{-4}]
 119 according to Koch et al. (2019) using Darcy-Forchheimer's law:

$$120 \quad \frac{\Delta P}{\Delta x} = - \left(\frac{\mu}{K} \right) q - \left(\frac{\rho}{K_1} \right) q^2 \quad (\text{Eq. 1})$$

121 where Δx is the stream wise depth of the vegetation, μ the viscosity of the fluid (Pa s), ρ the fluid density
 122 (kg m^{-3}), K_1 is the inertial permeability (m) and q the fluid flux (m/s), calculated as:

$$123 \quad q = v \varphi \quad (\text{Eq. 2})$$

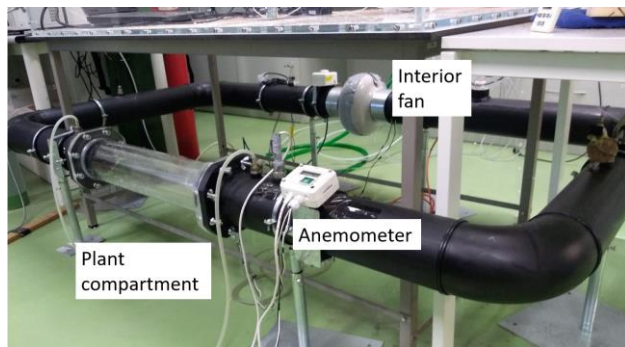
124 where v is the surface averaged wind speed in the duct (m s^{-1}) and φ the porosity (dimensionless). $\frac{\rho}{K_1}$ (kg
 125 m^{-4}) is the Forchheimer-drag coefficient. The dimensionless, normalized pressure loss ΔP_{norm} was
 126 calculated from:

$$127 \quad \Delta P_{\text{norm}} = \frac{\Delta P}{\rho v^2 \text{PAD} \Delta x} \quad (\text{Eq. 3})$$

128 where ρv^2 is a measure of kinetic energy per unit volume, also called the dynamic pressure (Pa).

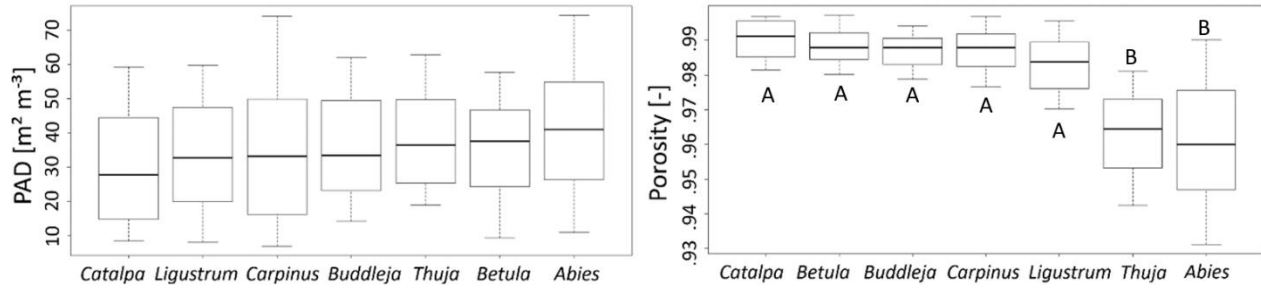
129 Normalised pressure loss for modelled data was plotted and compared to similar data from Koch et al.
 130 (2019) for herbaceous green wall species.

131



132
 133 Fig. 1: Wind tunnel setup

134



135
 136 Fig. 2: Left panel: Plant Area Density (PAD [$\text{m}^2 \text{m}^{-3}$]) values for each wind tunnel run per species. There are no
 137 significant differences in densities between species. Right panel: Porosity [-] values for each species. Significant
 138 differences are indicated with the letters A-B. Error bars represent minimum and maximum values.

139

140 2.3 CFD-MODEL

141 For all tree species, a CFD model was developed in COMSOL Multiphysics® version 5.2a (COMSOL Inc., MA,
 142 USA), based on porosity, permeability and Forchheimer-drag derived from the wind tunnel experiment.
 143 The geometry of the entire wind tunnel was applied as in Koch et al. (2019). The plant compartment was
 144 slightly wider than the other ducts. Considering the symmetry of the geometry, only half of the geometry
 145 was meshed as shown in Fig. 3. The computational grid consisted of approximately 170,000 tetrahedral
 146 cells with refinement at the boundaries. Grid size independency was ensured by gradually refining the
 147 mesh until further refinement did not affect the results. In this case, the average mesh quality of the
 148 geometry was 0.72. A relative tolerance of 0.0001 was used as convergence criterion. Only converged
 149 solutions were considered. Physics in the wind tunnel ducts were described as turbulent flow (k- ω
 150 incompressible flow at standard conditions [101325 Pa, 293.15 K]). In contrast to the laminar flow model,
 151 the k- ω model solves for extra variables: the turbulence kinetic energy and the rate of dissipation of
 152 turbulence kinetic energy ω . A steady-state solution was generated with a direct stationary solver (relative
 153 tolerance 0.001), by solving the governing equations of momentum and mass continuity in the wind tunnel
 154 ducts (Comsol 2017):

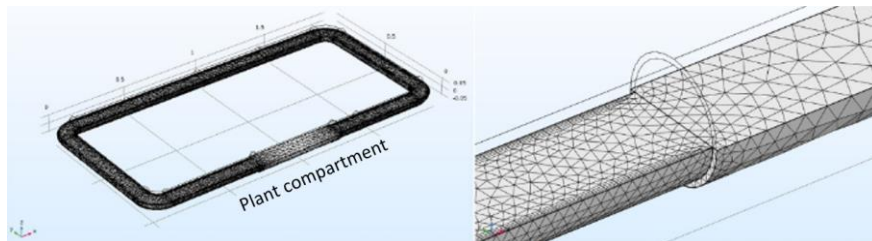
$$155 \quad \rho(\mathbf{u} \cdot \nabla)\mathbf{u} = \nabla \cdot \left(-P\mathbf{I} + (\mu + \mu_T)(\nabla\mathbf{u} + (\nabla\mathbf{u})^T) \right) \quad (\text{Eq. 4})$$

$$156 \quad \rho\nabla(\mathbf{u}) = \mathbf{0} \quad (\text{Eq. 5})$$

157 With ρ the air density (1.2044 kg m^{-3}), \mathbf{u} the velocity vector (m s^{-1}), \mathbf{I} an identity matrix, P the pressure
 158 (Pa), μ the dynamic viscosity (Pa s) and μ_T the eddy viscosity (Pa s), which is calculated by the k- ω model
 159 for a turbulent flow and equals zero in the case of a laminar flow. Second order discretisation was set by
 160 default in all equations.

161 For the plant compartment, Brinkman equations including Forchheimer-drag were applied (Eq. 1). As
 162 earlier research suggested these physics are the most suitable for determining air flow through vegetation
 163 (Molina-Aiz et al. 2006). To couple these two processes, pressures at the boundaries between the air ducts
 164 and the plant compartment were equalized. In Comsol, one can apply different physical processes (eg.

165 Brinkman's Law, turbulent air flow, ...) to different domains. In order to couple the physics at neighbouring
166 domains, boundary conditions should be defined and variables should be equal in order to connect the
167 different domains. This is a convenient and computationally profitable approximation for single phase fluid
168 flow in a porous medium (Bejan, 2013). A no slip condition was assumed at the walls. As mentioned earlier,
169 the static pressure curve of the fan was used as a single boundary condition. This means that the model
170 automatically finds the working point of the fan-duct system, corresponding to the pressure losses caused
171 by the vegetation and the duct walls. If plants are present in the tunnel, the pressure losses are higher,
172 shifting the working point of the fan more to the left of the graph (small Q and large ΔP). If the tunnel
173 is empty, pressure losses are low and the working point of the fan is on the right side of the graph. For a
174 detailed explanation on how this works, the authors refer to Koch et al. (2019) and to the book "Fluid
175 Mechanics: Fundamentals and applications, 4th edition". This means that the wind speed measured in the
176 experiment can later be used as a validation parameter, by comparing it with the modelled wind speed.
177 The same applies to the pressure loss measured by the pressure module and the modelled pressure loss.
178 The pressure losses, obtained by the model, were then compared with the experimentally measured
179 values to test the method.



180
181 Fig. 3: Geometry of the wind tunnel (left) and the computational mesh used in the model (right)

182

183 2.4 STATISTICAL ANALYSIS

184 All analyses were performed in R version 3.3.1 (<https://cran.r-project.org/>) and using an Excel worksheet.
185 Significance levels are always at 5%. An analysis of variance (ANOVA) was used to indicate significant
186 differences between species and their morphological parameters. Differences were indicated by a
187 TukeyHSD test which can be used to find means that are significantly different from each other. For
188 permeability and Forchheimer-drag, a log transformation was performed on the data because it was
189 skewed. To test whether permeability and Forchheimer-drag are normally distributed, a Shapiro-Wilk was
190 used. Both parameters scored high on the test (permeability: $W = 0.97691$, p -value = 0.01551;
191 Forchheimer-drag: $W = 0.95474$, p -value = 0.0001169), confirming a normal distribution. An ANOVA was
192 executed to look at the differences between the species and their permeability and Forchheimer-drag.
193 Differences were indicated by a Tukey-HSD test. Kendall rank correlations were performed to test the
194 correlations between permeability and Forchheimer-drag and PAD and porosity. Species morphological
195 parameters were compared with mean and median permeability and Forchheimer-drag by using ANOVA's.
196 Another ANOVA was performed to look at the differences between normalised pressure drops, together
197 with a Tukey-HSD to indicate the differences. Furthermore, to indicate differences between mean
198 normalized pressure drops and plant morphological parameters, an ANOVA was used.

199

200 **3 RESULTS**

201 **3.1 SPECIES MORPHOLOGY**

202 Table 3 shows an overview of all species morphological parameters and their standard deviations. An
 203 ANOVA indicated that FLS and LDI are negatively correlated ($p = 0.03994$). No other correlation between
 204 morphological parameters was found.

205 Table 3: Mean values of Functional Leaf Size (FLS), Leaf Dissection Index (LDI), Specific Leaf Area (SLA) and
 206 Leaf Size (LS) and their standard deviations (stdev) for the considered tree and shrub species. Species that
 207 significantly differ within a parameter are indicated by different letters a – f.

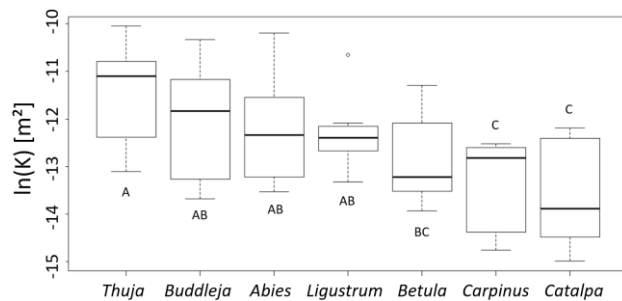
Species	mean FLS (-)	stdev FLS	mean LDI (-)	stdev LDI	mean SLA (m ² kg ⁻¹)	stdev SLA	LS (m ²)	stdev LS
<i>Abies</i>	1.15E-01 (d)	1.96E-02	7.38E+00 (a)	4.50E-01	4.72E+00 (e)	7.25E-16	2.47E-05 (d)	8.80E-06
<i>Betula</i>	7.50E-01 (a)	2.73E-02	5.50E+00 (a)	3.95E-01	1.08E+01 (d)	1.47E-01	1.00E-03 (bcd)	3.65E-04
<i>Buddleja</i>	3.76E-01 (c)	1.24E-01	5.81E+00 (a)	5.05E-01	2.14E+01 (a)	5.83E-01	1.83E-03 (bc)	1.76E-03
<i>Carpinus</i>	7.14E-01 (ab)	1.58E-01	5.65E+00 (a)	1.63E-01	1.33E+01 (b)	2.35E-01	1.59E-03 (bc)	7.45E-04
<i>Catalpa</i>	7.11E-01 (ab)	7.50E-02	4.69E+00 (a)	5.39E-01	1.26E+01 (c)	8.34E-01	1.02E-02 (a)	6.62E-03
<i>Ligustrum</i>	5.67E-01 (b)	9.49E-02	4.91E+00 (a)	3.27E-01	1.04E+01 (d)	3.61E-01	3.27E-04 (cd)	2.26E-04
<i>Thuja</i>	5.68E-02 (d)	4.74E-02	1.37E+01 (b)	3.81E+00	3.95E+00 (f)	8.55E-02	4.13E-04 (ab)	2.09E-04

208

209

210 **3.2 AERODYNAMIC CHARACTERISATION USING WIND TUNNEL EXPERIMENTS**

211 Permeability and Forchheimer-drag varied from 3.09×10^{-7} to $4.32 \times 10^{-5} \text{ m}^2$ and from 0.42 to 41.94 kg m⁻⁴, respectively. Differences in permeability are shown in Fig. 4. The ANOVA showed a significance of $p =$
 212 $3.138\text{e-}11$. No significant differences between species in Forchheimer-drag data were found ($p = 0.3571$).
 213



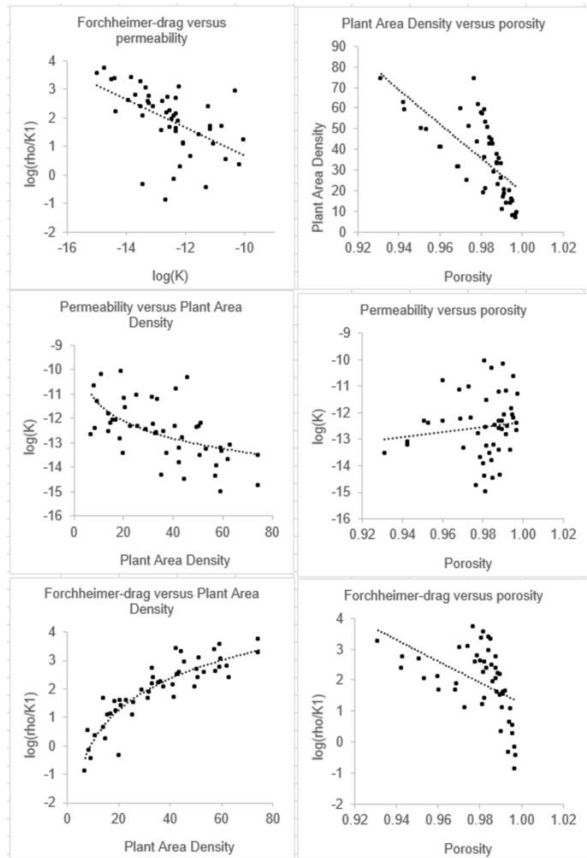
214

215 Fig. 4: Spread of permeability (natural log) values per species, classified from high to low median permeability.
 216 Significant differences are indicated with different letters A-C.

217

218 Kendall rank correlations are shown in Fig. 5. Permeability and Forchheimer-drag are strongly negatively
 219 correlated and PAD and porosity also. Both permeability and Forchheimer-drag are strongly correlated
 220 with PAD. Permeability is weakly positively correlated with porosity, while Forchheimer-drag is negatively
 221 correlated with porosity. Table 4 shows corresponding τ - and p -values and equations of the trend lines.

222



223

224 Fig. 5: Kendall rank correlations between permeability (K , m^2), Forchheimer-drag ($kg\ m^{-4}$), plant area density ($m^2\ m^{-3}$) and porosity (-). Each points represents one wind tunnel run for a specific species under different wind speeds.
 225
 226 Trend lines are also given (dotted line). Tau-values, p-values and equations of the trend lines are given in accessory
 227 table x.

228

229 Table 4: Accessory to Figure x: tau-values, p-values and equations of the trend lines shown in Fig. 4.

Forchheimer-drag versus permeability	Plant Area Density versus porosity
$\tau = -0.4698582$	$\tau = 0.3187921$
$p = < 2.2e-16$	$p = 2.548e-08$
$y = -0.4924x - 4.252$	$y = -795.3\ln(x) + 19.764$
Permeability versus Plant Area Density	Permeability versus porosity
$\tau = -0.3546099$	$\tau = 0.137134$
$p = 4.93e-10$	$p = 0.01657$
$y = -1.033\ln(x) - 9.0109$	$y = 9.7566x - 22.098$
Forchheimer-drag versus Plant Area Density	Forchheimer-drag versus porosity
$\tau = 0.09751773$	$\tau = -0.4719548$
$p = 0.08711$	$p = < 2.2e-16$
$y = 1.5974\ln(x) - 3.5284$	$y = -33.14\ln(x) + 1.2526$

230

231

232 3.3 CORRELATION BETWEEN AERODYNAMIC AND MORPHOLOGICAL
 233 PARAMETERS

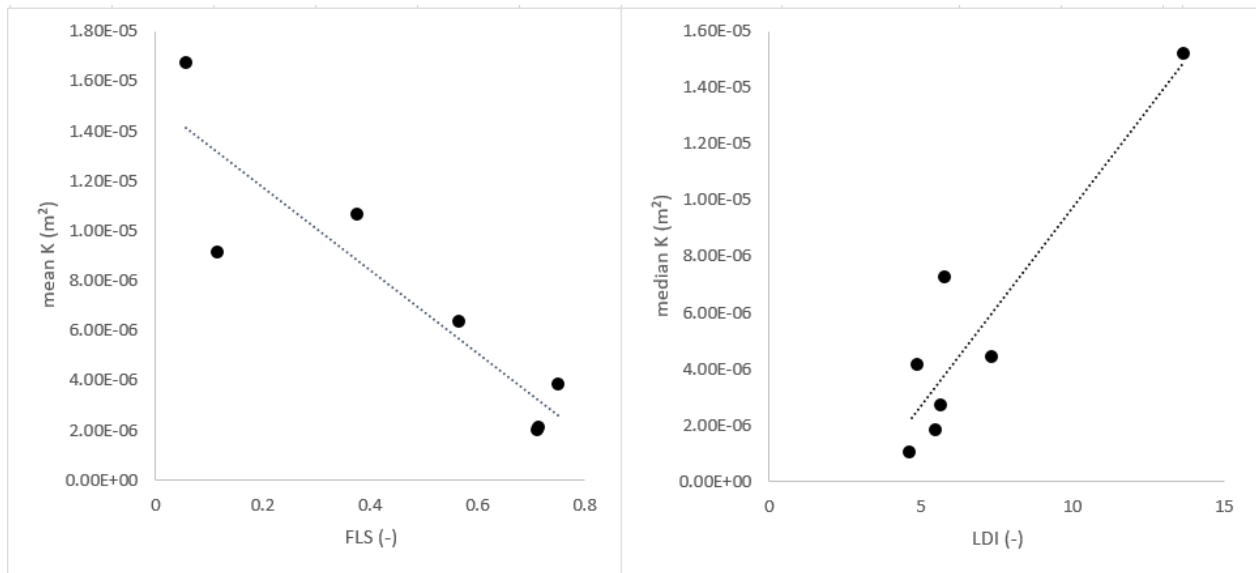
234 Correlations between mean and median permeability and Forchheimer-drag and the morphological
 235 parameters are given in Table 5. Table 5 shows that the variance in mean permeability can be explained
 236 by FLS and the variance in median permeability can be explained by LDI. Correlations are plotted in Figure
 237 6.

238
 239 Table 5: Morphological parameters Specific Leaf Area (SLA), Leaf Dissection Index (LDI), Functional Leaf
 240 Size (FLS) and Leaf Size (LS) as a function of permeability (K) and Forchheimer-drag (ρ/K_1). P-values of the
 241 correlations as result of an ANOVA are given. Stars indicate significant p-values ($p < 0.05$).

	Mean K	Mean ρ/K_1	Median K	Median ρ/K_1
SLA (m ² kg ⁻¹)	0.47	0.45	0.48	0.29
LDI (-)	0.02 *	0.20	0.0034 *	0.41
FLS (-)	0.0051 *	0.25	0.034 *	0.46
LS (m ²)	0.27	0.57	0.36	0.45

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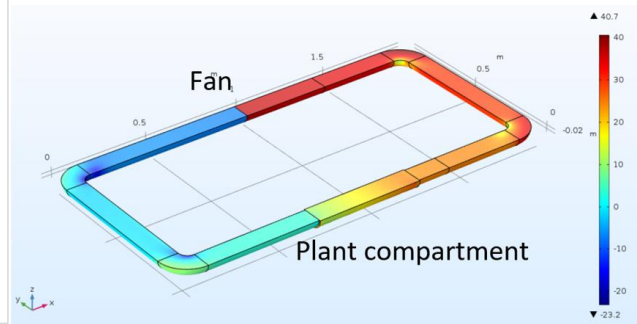
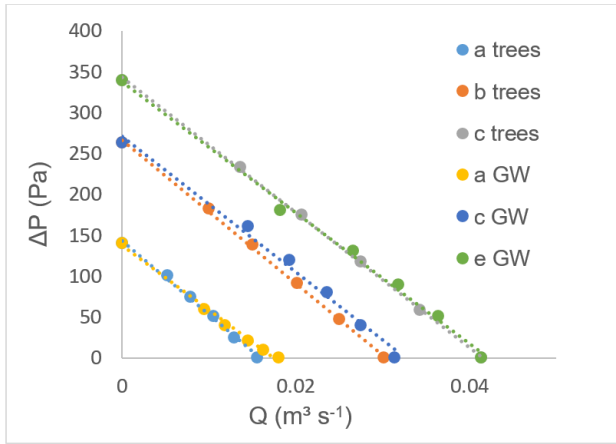
244

245 Fig. 6: Left: The correlation between Functional Leaf Size (FLS) (-) and the mean values for permeability K (m²).
 246 Equation of trend line: $y = -1.66 \cdot 10^{-5} x + 1.50 \cdot 10^{-5}$. Right: The correlation between Leaf Dissection Index (LDI) (-) and
 247 median values for permeability K (m²). Equation of trend line: $y = 10^{-6} x + 4 \cdot 10^{-6}$. Each point represents a species.
 248 Trend lines are shown as dotted lines. R² values of the trend lines are 0.82 (left) and 0.85 (right).

249

250 3.4 CFD-MODEL

251 Fan curves were derived from wind tunnel runs on three different fan power settings (see section 2.2). In
 252 Koch et al. (2019) the same was done on five different power settings (a to e) and results of both tests are
 253 given in Fig. 7. A typical result from the CFD model is given in Fig. 8. Other runs showed similar results.



254

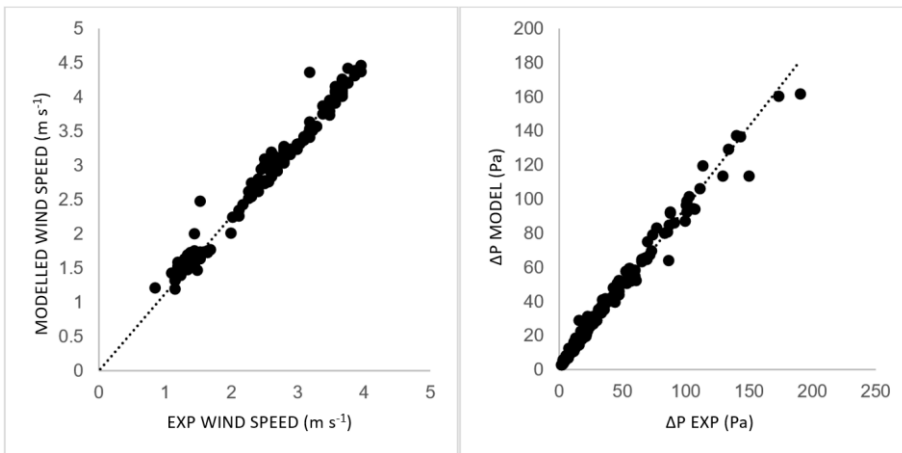
Fig. 7: Fan curve derived from trees (this paper) for three settings (a [low], b [middle] and c [high]) compared to fan curve derivation from Koch et al. (2018) for herbaceous green wall [GW] species (settings a, c and e).

Fig. 8: Typical pressure distribution obtained by the CFD model for the specific case of *Catalpa* ($PAD = 14.80 \text{ (m}^2 \text{ m}^{-3}\text{)}$, $\varphi = 0.9955$, $K = 5.0907 \cdot 10^{-6}$, $\rho/K1 = 1.3007 \text{ kg m}^{-4}$)

255

256

257 The model was validated by plotting the measured average wind speed over the cross-section of the tunnel
 258 by the anemometer against the simulated wind speed at the exact position of the anemometer (Fig. 9 left
 259 panel), also integrated and averaged over the cross-section of the tunnel. Given that the fan was the only
 260 boundary condition (see section 2.2), this is a reliable method. A good agreement between model and
 261 experiment was found ($R^2 = 0.98$). The same applies to pressure loss data, as the modelled pressure loss
 262 corresponds well to experimental pressure loss (Fig. 9 right panel).

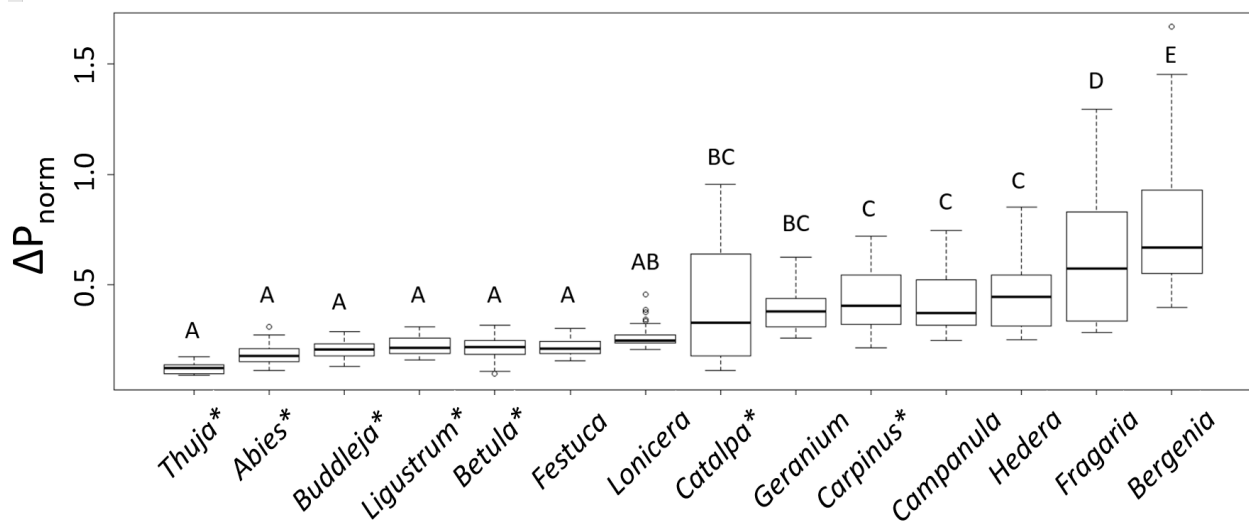


263

264 Fig. 9: Scatter plot of all experimental versus modelled data. Each dot represents a specific wind tunnel run. The
 265 dotted lines represent the trend lines. Left panel: relationship between measured (exp) and modelled wind speed.
 266 Equation: $y = 1.1284x$, $R^2 = 0.98$. Right panel: modelled versus experimental pressure loss (ΔP). Equation: $y = 0.95x$,
 267 $R^2 = 0.98$.

268

269 Figure 10 shows a ranking for normalized pressure losses (ΔP_{norm}) of the considered tree species
 270 supplemented with data from Koch et al. (2019) on herbaceous green wall species. Because of the good
 271 correlation of experimental and modelled pressure losses (Fig. 9 right panel), only modelled values are
 272 shown. Even though a normalization for air and plant density, wind speed and stream wise depth of the
 273 plant compartment was performed (Eq. 3), clear differences can be seen between species and significantly
 274 different groups (p-value of $< 2.2 \cdot 10^{-16}$) can be distinguished (A-E). The first group consists of five species
 275 (*Thuja*, *Abies*, *Buddleja*, *Ligustrum*, *Betula* and *Festuca*), while e. g. *Catalpa* and *Carpinus* have clearly much
 276 higher values. The figure shows that in general tree species have a lower score for ΔP_{norm} values, as well as
 277 a smaller range, where herbaceous species have higher values and wider ranges for normalised pressure
 278 drop. For every species a mean normalised pressure loss was calculated for modelled values in order to
 279 test against morphological parameters. An ANOVA showed that no variance in normalised pressure loss
 280 could be explained by either one of the considered morphological parameters on their own or by
 281 interactions.



282
 283 Fig. 10: Normalised pressure losses for tree and shrub species used in this paper (indicated with a *) and for
 284 herbaceous green wall species as reported in Koch et al. (2019). Significant differences are indicated with the letters
 285 A-E.

286

287 4 DISCUSSION

288 4.1 WIND TUNNEL EXPERIMENTS

289 In general, wind tunnel studies are convenient because several environmental variables can be controlled,
 290 which makes it interesting for providing data for validating model simulations. Moreover, in the case of
 291 this research, edge effects of airflow on a vegetation stand are minimized, because the wind tunnel is
 292 entirely filled, and air is forced to go through the vegetation. In contrast, most wind tunnel studies describe
 293 airflow around vegetation, where other flow patterns occur.

294 Tree and shrub branches of different porosities, ranging from 93.1% (*Abies*) to 99.7% (*Betula*) (Fig. 2 right
 295 panel) were brought into the wind tunnel. This is a wider range than Gromke & Ruck (2012), who found

296 porosities of 96 to 97.5%. Lin et al. (2012) found in a similar experiment with variable packing densities
297 (volume vegetation/volume wind tunnel) of 0.037 and 0.055 for Juniper and 0.017 and 0.040 for Pine. Our
298 packing densities varied in a wider range, from 0.002 (*Betula*) to 0.069 (*Abies*). In addition, earlier research
299 within the department showed values for permeability and Forchheimer-drag of $3.8 \times 10^{-7} \text{ m}^2$ and 29 kg
300 m^{-4} , respectively and a porosity above 99% for fiberglass. These values fall into the range of this study
301 (permeability from 3.1×10^{-7} to $4.3 \times 10^{-5} \text{ m}^2$ and Forchheimer-drag from 0.4 to 41.9 kg m^{-4}), which implies
302 that fiberglass could be deployed to simulate certain plant species. Similarly to the findings of Koch et al.
303 (2019), permeability seemed to be influenced by species (Fig. 4), but Forchheimer-drag did not, even
304 though roughly the same ranges of densities (Fig. 2 left panel) were used per species. The differences in
305 permeability could partially be explained by some leaf morphological parameters, namely FLS and LDI,
306 which had a negative and positive correlation with mean permeability and median permeability,
307 respectively (Fig. 6). This means that permeability can be (partially) predicted by looking at a species' leaf
308 shape, more specifically its degree of roundness and serration. These results are different from, but not
309 contradictory to the findings in Koch et al. (2019), where correlations between permeability and SLA, and
310 Forchheimer-drag and FLS were found.

311 Figure 5 (centre, left) shows a logical agreement between permeability and PAD, as more plant material is
312 less penetrable by air. This is in accordance to Sase et al. (2012). It also shows a correlation of permeability
313 with Forchheimer-drag (Fig. 5 top, left), which means Forchheimer-drag can be estimated from
314 permeability data. Furthermore, a correlation was found between Forchheimer-drag and PAD (Fig. 5
315 bottom, left). This indicates that by considering only plant density, the Forchheimer-drag can be estimated.
316 This correlation is also logical because more plant material means more air flow being blocked, which
317 results in higher turbulence and inertia. Figure 5, top right, shows a negative correlation of PAD and
318 porosity. This makes sense, since both parameters are related to the amount of plant material present,
319 but in an opposite way. Porosity and permeability are positively related since the presence of more void
320 spaces facilitates the air flow through the vegetation. On the other hand, Forchheimer-drag has a strong
321 negative correlation with porosity, which indicates that drag forces are more important when the
322 vegetation is packed more densely.

323

324 4.2 MODEL VS. EXPERIMENT

325 In general, CFD models provide a fast, cheap and easy way to assess physical processes. They can be used
326 on micro- or full scale and are able to rule out environmental variables which can make it difficult to
327 compare experiments, such as meteorological conditions. Figure 9 (right panel) shows a good correlation
328 between modelled and experimental pressure drops, which means that the Darcy-Forchheimer model is
329 a good proxy for what happens with wind flow through vegetation for woody species that are considered
330 as trees and shrubs. Consequently, it is safe to assume this model works for a wide diversity of woody and
331 herbaceous plant species. Validation with wind speed also indicates a good fit between model and
332 experiment.

333 After normalization for air and plant density, wind speed and stream wise plant depth, a clear pattern in
334 pressure losses could be found between species (Fig. 10). This would be expected to be caused by species-
335 specific morphological characteristics. Nevertheless, even after addition of data from Koch et al. (2019),
336 no correlations with the considered morphological parameters could be found. Because of these findings,
337 we assume that the transfer of impulse is an important factor influencing the pressure loss. Depending on

338 the rigidity of the vegetation structures, wind energy is partially converted into branch and leaf movement,
339 resulting in an additional pressure loss that was not considered in the study. It was clearly observed that
340 there were vibrations of leaves and thin branches during the experiments, even at the lowest air speed.
341 Investigating the effect of rigidity would demand experiments to be performed at even lower air speeds,
342 which was not possible with the equipment used. Also, rigidity or stiffness tests of the vegetation material
343 should be conducted using a stiffness tester or similar device. We believe that such research would lead
344 to important new insights on the aerodynamics of vegetation. In a rigorous approach, leaves and branches
345 can be considered as multiple masses connected by springs and dampers, where also rotational inertia is
346 involved.

347 It is therefore proposed that further research should include the transfer of impulse, along with the Navier-
348 Stokes equations and the transfer of energy to heat due to viscous effects. This is a challenging task as the
349 transfer of impulse depends on other parameters that were not considered in this work, for example the
350 rigidity of the vegetation structures. However, plant permeability can be (partly) predicted by assessing a
351 species' leaf shape, more specifically LDI and FLS. On the other hand, PAD was found to be a determining
352 factor for Forchheimer-drag.

353 5 CONCLUSIONS

354 This study suggests that the Darcy-Forchheimer approach works for describing air flow through multiple
355 types of vegetation. Consequently, it can be used for modelling the interactions between atmosphere and
356 environment and contribute to a wider knowledge on this topic. The Darcy-Forchheimer approach can be
357 considered a holistic approach because it covers the integrated effect of leaves, stems, branches and their
358 size, shape, density and rigidity.

359 Moreover, plant species can be classified under a range of pressure drops normalised for density. In other
360 words, there is a difference in normalised pressure drop between species that cannot be explained by the
361 used leaf morphological parameters. It is proposed that further research into kinetic energy transfer based
362 on rigidity factor is carried out. However, plant permeability can be (partly) predicted by assessing a
363 species' leaf shape, more specifically LDI and FLS and PAD was found to be a determining factor for
364 Forchheimer-drag.

365

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370

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